ASC-TR-95-1004

MARK IIA AQUEOUS FILM FORMING FOAM (AFFF) PRECISION METERING SYSTEM PRODUCT EVALUATION TEST REPORT

Aeronautical Systems Center Weapons, Air Base and Range Product Support Office ASC/VXO 314 W. Choctawhatchee Ave., Ste. 104 Eglin AFB FL 32542-5717



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ABBREVIATIONS/ACRONYMS/SYMBOLS

AQUEOUS FILM FORMING FOAM AFFF AFR AIR FORCE REGULATION

ARA APPLIED RESEARCH ASSOCIATES, INC.

AIRCRAFT RESCUE AND FIREFIGHTING VEHICLE ARFF

Αo OPERATIONAL AVAILABILITY

BDM MANAGEMENT SYSTEMS COMPANY BDM

DEPARTMENT OF DEFENSE DOD

DSN DEFENSE SWITCHING NETWORK

GALLONS PER MINUTE gpm

IN ACCORDANCE WITH **IAW**

LIMITED TECHNICAL INSPECTION LTI

THE COMPUTERIZED FOAM PROPORTIONING SYSTEM (PRODUCED BY MARK IIA

NORDIC SYSTEMS INC.)

MDT MEAN DOWN TIME

MTBM MEAN TIME BETWEEN MAINTENANCE

NFPA NATIONAL FIRE PROTECTION ASSOCIATION

P-19 A/S32P-19 CRASH FIRE RESCUE VEHICLE

PROGRAM MANAGEMENT DIRECTIVE PMD

RM&A RELIABILITY, MAINTAINABILITY, AND AVAILABILITY

RESPONSIBLE TEST ORGANIZATION RTO

WRIGHT LABORATORY/ AIRBASE FIRE PROTECTION AND CRASH WL/FIVCF

RESCUE SYSTEMS SECTION

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SECTION I PURPOSE AND BACKGROUND

- 1.0 **PURPOSE.** The purpose for this product evaluation was to examine an off-the-shelf aqueous film forming foam (AFFF) metering system for incorporation on Air Force Crash Fire Rescue Vehicles. This product evaluation was accomplished as part of a continuing effort to identify an AFFF system capable of metering foam accurately at 1%, 3% and 6% concentrations. The results of this evaluation will support a decision to apply the technology to Air Force firefighting apparatus. If applicable, the Department of Defense (DOD) could use the results of the evaluation for other firefighting vehicles.
- 1.1 <u>AUTHORIZING DIRECTIVES</u>. Authority for the Mark IIA system product evaluation is in PMD 8028(9), dated 10 May 1991. This evaluation was conducted as directed in AFR 80-14 and AFR 55-43.
- 1.2 BACKGROUND. The DOD currently uses AFFF concentrates formulated and mixed with water in ratios of 3 and 6 percent, using an around-the-pump proportioning system with fixed orifices. Common fire protection community terminology refers to an AFFF concentrate designed to be mixed with water at a ratio of 3% AFFF to 97% water as "3% AFFF". A "6% AFFF" concentrate contains approximately one-half of the surfactant and other active ingredients as 3% AFFF concentrate per unit volume and, consequently, is referred to as "less concentrated". When mixed with water at their designed ratios, both types AFFF/water mixture are essentially the same. The newest commercial AFFF formulation is 1% concentrate which is increasingly being used by civilian firefighting facilities. By using 1.0% AFFF concentrate (as compared to 3% and 6%), a considerable cost savings in shipping and storage can be achieved. Likewise, agent conservation, extended firefighting capability, and reduced environmental impact can be realized. Although the Air Force inventory is 3% AFFF, 6% foam concentrate was evaluated to provide system performance data when the Air Force must acquire 6.0% foam such as was done during Operation Desert Shield/Storm. To enhance the interoperability of Air Force firefighting equipment during contingency applications, an additional capability to use 1% AFFF is highly advocated.
- 1.3 <u>DESCRIPTION OF SYSTEM TESTED</u>. The Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System (hereafter called the Mark IIA) is a computer controlled metering system that continually adjusts the foam flow to deliver the correct solution concentration. Nordic Systems Inc. personnel installed and calibrated the Mark IIA system on a WL/FIVCF P-19 firefighting vehicle and provided operator and maintenance training to evaluation participants. The Mark IIA system consists of: a computer, foam flow meter, solution flow meter, foam control valve, self-contained digital read-out unit, and associated wiring and electrical connectors. A follow-on test phase replaced the paddle wheel flow meters for water and AFFF with magnetic flow meters. The advantages of the magnetic flow meters are more consistent metering and higher maintenance reliability. The

Mark IIA computer program has been modified to meet current USAF objectives to provide foam in concentrates of 1%, 3%, and 6% at flow rates between 60 and 750 gallons per minute (GPM). The AFFF dispensing ratio of the Mark IIA system is switch selectable over a range of 0-6% AFFF by the operator from the cab of the vehicle. When the AFFF reservoir is refilled with foam concentrate, the vehicle operator can adjust the Mark IIA to match the AFFF concentration in the reservoir.

1.4 <u>TEST FORCE, LOCATION, DATES</u>. Wright Laboratory, Airbase Fire Protection and Crash Rescue Systems Section (FIVCF), managed this product evaluation to verify metering accuracy, operational effectiveness, and suitability of the Mark IIA. The initial evaluation was conducted by the Responsible Test Organization (RTO), WL/FIVCF, between 16 December 1992 and 25 June 1993, at Tyndall AFB, FL. The follow-on evaluation of the magnetic flow meters was conducted between 7 and 9 November 1994.

SECTION II PRODUCT EVALUATION DESCRIPTION

- 2.0 <u>OBJECTIVES</u>. WL/FIVCF used the data collected to compare the AFFF metering accuracy of the Mark IIA with the orifice plate system currently employed on the P-19. The primary objective of this evaluation was to verify the AFFF metering accuracy and consistency of the Mark IIA system in the P-19 firefighting vehicle. This evaluation assessed the Mark IIA system performance, operational effectiveness, and suitability for use with the P-19.
- 2.0.1 <u>Objective E-1</u>. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- 2.0.2 <u>Objective E-2</u>. Assess the operational performance of the Mark IIA system installed on the P-19.
- 2.0.3 Objective S-3. Assess the compatibility of the Mark IIA system installed on the P-19 with firefighting operations.
- 2.0.4 <u>Objective S-4</u>. Assess the adequacy of technical data provided with the Mark IIA system.
- 2.0.5 Objective S-5. Assess the Mark IIA system Reliability, Maintainability and Availability (RM&A).
- 2.1 SCOPE AND METHOD OF ACCOMPLISHMENT. Prior to modifying the P-19 vehicle with the Mark IIA system, the RTO demonstrated the AFFF metering accuracy of the existing orifice plate system for 1%, 3% and 6% AFFF. The performance baseline was established for comparison with the Mark IIA system. After the orifice plate system was baselined, the Mark IIA system was installed on the same P-19 vehicle and the same AFFF metering accuracy data was collected. At the conclusion of each foam percentage evaluations, the AFFF metering accuracies were measured using sight gauges to evaluate the repeatability of the Mark IIA system to consistently provide 1%, 3%, and 6% AFFF. When the magnetic flow meters were installed, their performance was verified by an in-line mechanical measuring meter.

The evaluation participants from FIVCF/ARA were task qualified firefighting and maintenance personnel. General firefighting practices and procedures as outlined in National Fire Protection Association Standard 412, Evaluating Aircraft Rescue and Foam Fire Fighting Equipment, were followed.

Mark IIA system reliability data are reported as mature system point data since the system is commercially available (off-the-shelf).

2.2 <u>PLANNING CONSIDERATIONS AND LIMITING FACTORS</u>. Only one A/S32P-19 Crash Fire Rescue Vehicle was modified for this test. The baseline metering performance of the P-19 examined 1%, 3% and 6% AFFF dispensing; however, manufactured orifice plates were available only for 3% and 6%. Former attempts to meter at 1% using an orifice plate were unsuccessful. For this test, WL/FIVCF//ARA fabricated a 1% orifice plate to establish a baseline for evaluating the Mark IIA system.

The paddle wheel flow transducer in the Mark IIA system used to measure the flow of foam is accurate between a minimum of 2.7 GPM and a maximum of 81 GPM. The magnetic flow meter used in the second phase of testing measures between 0.2 and 100 GPM. This means that during the first phase of testing, when using the bumper turret only with 1% AFFF, or when using the hand line only at 1% or 3% AFFF, the mixture will be slightly inaccurate. To more reliably measure the quantities of AFFF solution used in these cases, a small auxiliary tank was installed with a more precise measurement scale. This auxiliary tank was not in place during the baseline runs with the orifice plates.

SECTION III EFFECTIVENESS AND SUITABILITY

- 3.0 SUMMARY. The Mark IIA system was evaluated as specified in the test plan. Data on system performance, operational effectiveness and suitability were recorded as point data due to the relatively short evaluation period. The P-19 vehicle water and AFFF tanks were calibrated. The P-19 and Mark IIA systems were serviced and prepared for use in accordance with applicable technical manuals. After preparation for use, the P-19 and Mark IIA systems were operated to dispense AFFF ten times from each turret/nozzle (roof, bumper, and handline) for 60 seconds with 1%, 3%, and 6% AFFF. After each dispensing operation, the water and AFFF tank quantities were recorded using fluid sight gauges on the vehicle to determine the amounts used. This was accomplished to compute the Mark IIA system metering accuracy and to determine repeatability with the various AFFF concentrations. In the second phase (with magnetic flow meter) each turret/nozzle was operated five times each. The handline was included to determine the Mark IIA's ability to accurately meter AFFF at low flow rates. Since the dispersal pattern is primarily determined by the turret/nozzle and has been previously established, this test evaluated only the mixture of foam concentrates. No dispersal patterns were measured or pit fires extinguished. Special attention was given to the Mark IIA system performance. Nordic Systems technicians assisted FIVCF personnel during the installation and calibration of the Mark IIA system in the P-19 evaluation vehicle. They performed a limited technical inspection (LTI) and functionally operated the Mark IIA modification prior to beginning the evaluation. FIVCF/ARA/BDM personnel compared the installed hardware and components to the technical data package provided by Nordic Systems Inc. to verify completeness. During initial test and calibration, the measurement accuracy for small quantities of foam was inconsistent. On 8 Mar 93, an auxiliary 10-gallon foam tank was added to the P-19 to provide a more precise measurement container for low foam rate delivery test events.
- **3.1** Objective E-1. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- **3.1.1** <u>Method.</u> Nordic Systems technicians assisted FIVCF personnel in the installation and calibration of the Mark IIA system in the P-19 evaluation vehicle. They performed a limited technical inspection (LTI) and functionally operated the Mark IIA modification prior to beginning the evaluation. Nordic gathered performance data and modified the Mark IIA computer program to conform with the exhibited characteristics of the P-19 installation. FIVCF/ARA/BDM personnel compared the installed hardware and components to the technical data package provided by Nordic Systems Inc. to verify completeness.
- **3.1.2** Results and Conclusions. During the installation, pictured in Appendix C, some adjustments to the data package were necessary to reflect the actual parts and location of items on this model of the P-19. The computer metering program had to be updated once calibration runs were accomplished. The final data package accurately represents the procedures and techniques required to modify the P-19 with the Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System.

- 3.1.3 Recommendations. None.
- **3.2** Objective E-2. Assess the operational performance of the Mark IIA system installed on the P-19.
- 3.2.1 Method. The P-19 vehicle water and AFFF tanks were calibrated following the Firefighting Vehicle Fluid Calibration Procedures in the test plan. The P-19 and Mark IIA systems were serviced and prepared for use in accordance with applicable technical manuals. The P-19 and Mark IIA systems were operated to dispense AFFF ten times from each turret/nozzle (roof, bumper, and handline) for 60 seconds with 1%, 3%, and 6% AFFF. After each dispensing operation, the water and AFFF tank quantities were recorded from fluid sight gauges on the vehicle to determine the amounts used. These readings were used to compute the Mark IIA system metering accuracy and repeatability with the various AFFF concentrations. The handline was included to determine the Mark IIA's accuracy at low flow rates. During dispensing operations, special attention was given to the Mark IIA system performance.
- 3.2.2 Results and Conclusions. The Mark IIA system on the P-19 fire truck performed excellently during all phases of the evaluation. Consistent performance was difficult at the low foam flow rates. More consistent measurements were achieved using the magnetic flow meters. Metering results are summarized in Table 1 and elaborated in Figures 1 through 3. When the magnetic flow meters were installed for the second phase, the computer control had to be modified, but time and field equipment did not allow optimizing the control system. The mixture was slightly rich for all magnetic flow meter performance. In the graphs of figures 1 through 3, the left group of results are for the baseline runs, the center group is the NORDIC IIA system with paddlewheel flow meters and the right hand group is performance with the magnetic flow meters. Operationally, when the foam tank is refilled with foam of a different concentration than had been previously dispensed, the ratio of foam dispensed can be changed from inside the vehicle cab by a single switch change, providing a real time read-out of foam concentration being delivered at the dispensing nozzle. Currently a change in foam concentration requires a change in the orifice plate, a nominal 1.5 hour procedure.
- **3.2.3** Recommendations. An accurate calibration of all components in a kit should be accomplished at the production facility. If recalibration is necessary after repair actions in the field, a procedure should be incorporated in the technical order.

Table 1
Average AFFF metering system performance

	1% AFFF	3% AFFF	6% AFFF
*	0.9 - 1.2	2.8 - 3.5	5.5 - 7.0
Target Range		(2.8 - 4.0 Handline)	(5.5 - 8.0 Handline)
ROOF			
Baseline	1.1	3.8	6.7
Mark IIA	1.0	3.1	6.4
Magnetic Flow Meters	1.1	3.3	6.2
ROOF & BUMPER			
Baseline	1.1	3.8	6.5
Mark IIA	0.9	3.1	6.1
Magnetic Flow Meters	1.1	3.2	6.0
BUMPER			
Baseline	0.9	2.9	6.7
Mark IIA	1.2	2.7	6.0
Magnetic Flow Meters	1.2	3.5	6.8
HANDLINE			
Baseline	1.1	3.7	5.2
Mark IIA	1.7	2.8	5.9
Magnetic Flow Meters	2.1	3.6	6.8

Target ranges for 3% and 6% AFFF have been established in NFPA Standard 412, the target range for 1% has not been established by NFPA but was introduced by applying criteria similar to the 3% and 6% ranges.

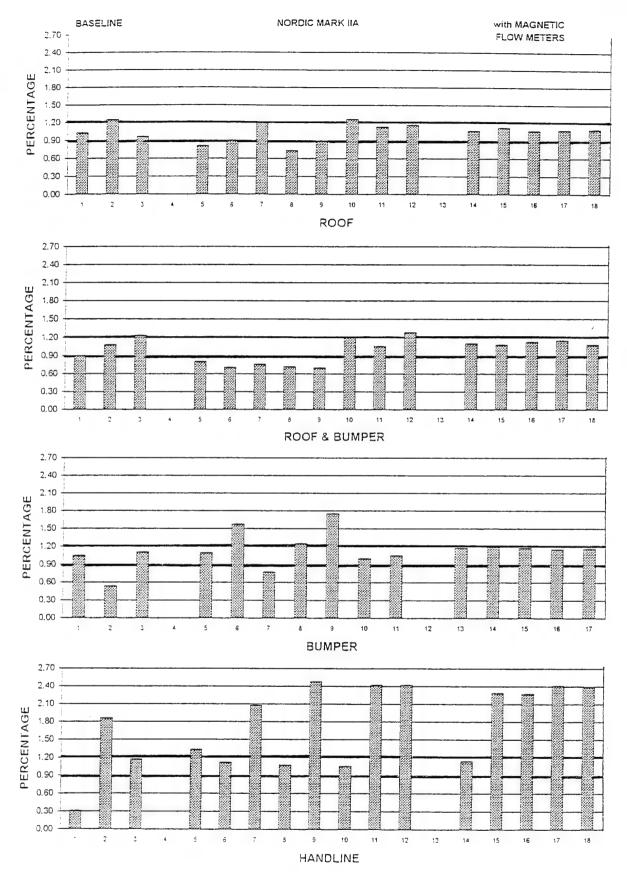


Figure 1 1% AFFF Performance Target Range 0.9 - 1.2%

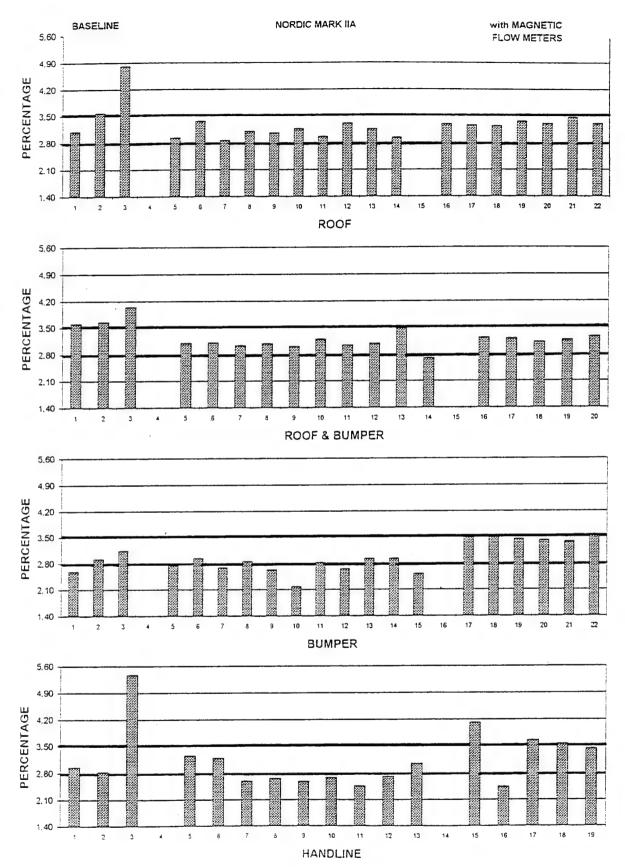


Figure 2 3% AFFF Performance Target Range 2.8 - 3.5%

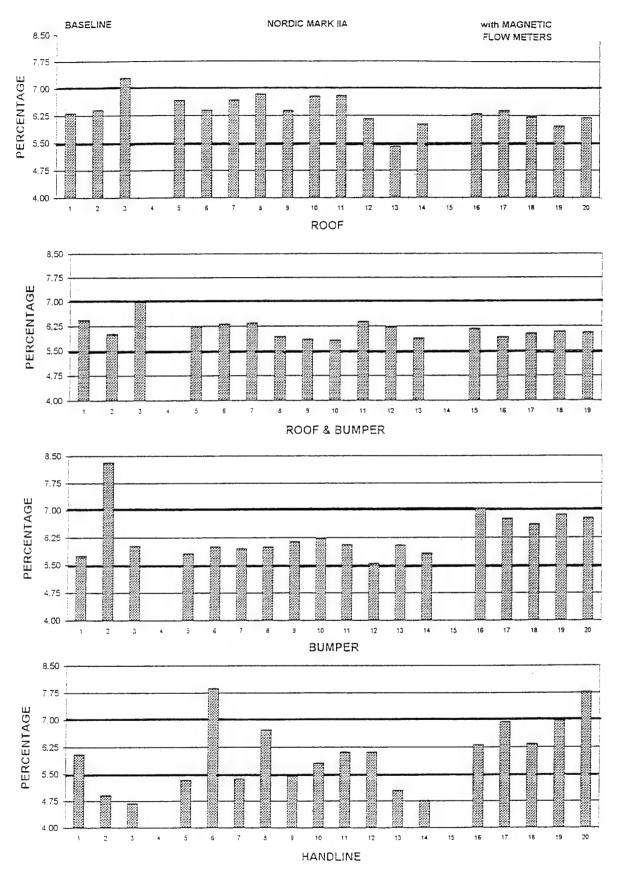


Figure 3 6% AFFF Performance Target Range 5.5 - 7.0%

- **3.3** Objective S-3. Assess the compatibility of the Mark IIA system with the P-19 firefighting vehicle.
- **3.3.1** Method. The Mark IIA system was employed as described in the test plan and maintained IAW the operational concept and the manufacturer's technical data. The evaluation participants were briefed to be alert for any actual or foreseeable compatibility problems between and among the components and to notify the Evaluation Manager of any observed or experienced compatibility problems.
- 3.3.2 <u>Results and Conclusions</u>. No incompatibilities between the Mark IIA system and the P-19 fire truck were noted. Once the system was installed, changing to a different foam concentration required a single switch change instead of the nominal 1.5 hours previously required to change orifice plates. From a firefighters perspective, operations using the metering system were transparent to using the orifice plate system. With this type of metering system installed, the P-19 becomes more versatile due to its expanded capability to operate using 1% foam concentrate. The addition of this system makes the Air Force A/S32P-19 Crash Fire Rescue Vehicle or any other fire vehicle better suited for worldwide contingency operations using stockpiles of differing foam concentrations.
- **3.3.3** <u>Recommendations</u>. Investigate retrofit installation of a computerized metering system on all Air Force Fire/Crash Rescue vehicles that use AFFF as their primary firefighting agent.
- **3.4** Objective S-4. Assess the adequacy of the vendor provided technical manuals for the Mark IIA system.
- **3.4.1** Method. During this evaluation, participants used the vendor provided technical manuals. After each evaluation event, the participants indicated, on data forms and maintenance logs, any difficulties that prevented or hindered successful task performance. The Evaluation Manager recorded pertinent observations and comments in the Evaluation Manager's Log. The technical manual was reviewed and verified.
- **3.4.2** Results and Conclusions. During the installation, some adjustments to the data package were necessary to reflect the actual parts and location of items on this model of the P-19. The final data package accurately represents the procedures and techniques required. Operating instructions for the Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System were clear and adequate for the necessary control settings and adjustments.
- **3.4.3** Recommendations. The next kit installed should serve as a kit proofing to verify that the data package is appropriate for base or depot level modification, depending upon where system installations will be accomplished.

- **3.5** Objective S-5. Assess the Mark IIA system Reliability, Maintainability, and Availability (RM&A).
- **3.5.1** <u>Method</u>. The Evaluation Manager and participants recorded any system failures and repair data. These data were to serve as the basis to calculate system point RM&A rates for the evaluation period.
- 3.5.2 Results and Conclusions. After the magnetic flow meters were installed, the computer controlled foam metering valve was operating erratically. The valve was replaced to provide accurate test results. This component was a manual valve that the contractor (NORDIC) had modified to be controlled by an electric motor. Since that phase of testing, the valve has been replaced by a commercially produced motorized valve made by Elkart. No system failures occurred during the evaluation period and no repairs were required. The first phase of test consisted of 32 hours of operation. The vehicle was in use for 16 months between phases and the system accumulated 56 hours of test operation by the conclusion of testing. This length of documented test operation is inadequate to provide any long term RM&A data. Mean Time Between Maintenance (MTBM) and Mean Down Time (MDT) could not be calculated since no records account for the amount of use during the 16 months between test phases. Operational Availability (Ao) was 100% during the periods of this evaluation.
- **3.5.3** <u>Recommendations.</u> If representative RM&A data are required, recommend a number of systems be installed in operational units and operated for a minimum of six months.

SECTION IV SUMMARY OF CONCLUSIONS AND RECOMMENDATIONS

- 4.0 Conclusions. During the installation, some adjustments had to be made to the plumbing and data package. The final data package outlines the requirements to modify the P-19 with the Mark IIA System. Consistent performance was difficult at the low foam flow rates. More consistent measurements were achieved by using magnetic flow meters. When the foam tank is refilled with foam of a different concentration than has been previously dispensed, the ratio of foam dispensed can be changed from inside the vehicle by a single switch change instead of the nominal 1.5 hours previously required to change orifice plates. A real time read-out of foam dispensing concentration is presented to the operator. No incompatibilities between the Mark IIA system and the P-19 fire truck were noted. From a firefighters perspective, operations using the metering system were transparent to using the orifice plate system. With this type of metering system installed, the P-19 becomes more versatile due to its expanded capability to operate using 1%, 3% and 6% foam concentrate. The addition of this system makes Air Force Crash Fire Rescue Vehicles better suited for worldwide contingency operations. Operating instructions for the Mark IIA were clear and adequate for the necessary control settings and adjustments. No system failures occurred during the evaluation period and no repairs were required. The test events, completed during 56 hour of operation, were inadequate to provide any long term RM&A data. Operational Availability (Ao) was 100% during the period of this evaluation.
- **4.1** Recommendations. Recommend that a computerized foam metering system be competitively procured for field and/or depot retrofit of P-19, P-23, and other front line ARFF vehicles. If a system calibration is required after field level repair, a procedure should be added to the technical order. If representative RM&A data is required, recommend a number of systems be installed in operational units and operated for a minimum of six months.

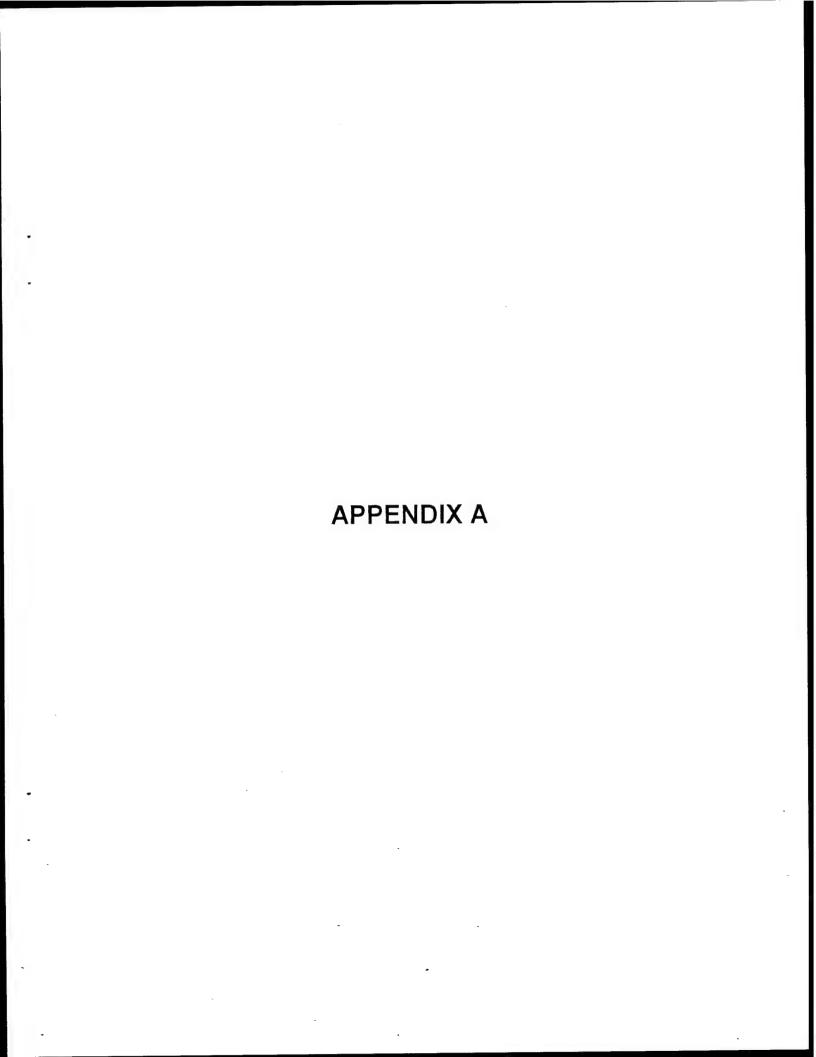


Table A-1 P-19 fluid tank calibration table

Wate	er Tank	Fill	AFF	Tank	Auxiliary	AFFF Tank
Quantity Gallons	Depth in inches	Point	Quantity Gallons	Depth in inches	Quantity Gallons	Depth in inches
0	8	1	0	19	0	0
50	10 1/2	2	5	21 1/16	1	2 15/16
100	12 5/16	3	10	22 3/8	2	5 7/8
150	15 5/16	4	15	23 9/16	3	8 13/16
200	17 5/8	5	20	24 3/16	4	11 3/4
250	20	6	25	24 15/16	5	14 11/16
300	22 3/16	7	30	25 5/8	6	17 5/8
350	23 15/16	8	35	26 5/16	7	20 19/32
400	25 1/2	9	40	27 1/8	8	23 17/32
450	27 3/16	10	45	27 15/16	9	26 15/32
500	28 7/8	11	50	28 5/8	10	29 13/32
550	30 9/16	12	55	29 5/8	11	32 11/32
600	32 1/4	13	60	29 15/16	12	35 9/32
650	33 15/16	14	65	30 5/8		
700	35 9/16	15	70	31 3/8		
750	37 5/16	16	75	32		
800	39	17	80	32 5/8		
850	40 5/8	18	85	33 3/8		
900	42 1/4	19	90	34 1/16		
950	43 15/16	20	95	34 3/4		
1000	45 5/8	21	100	35 3/8		
		22	105	36 1/8		
		23	110	36 3/4		
		24	115	37 9/16		
		25	120	38 1/8		
		26	125	38 7/8		
		27	130	39 13/16		

APPENDIX A NORDIC MARK IIA EVALUATION MATRIX AND RESULTS

FIGURE	1			PLANNED ACTUAL WATE					TER TANK AFF						Γ	CALC.
FIGURE	TEST		AFFF	DISPENSING		INC	HES		ONS	INC	CHES		LONS	WATER	AFFF	RATIO
NO.	NO.	TURRET	TANK	TIME (sec)	TIME (sec)	START	END	START .	END	START	END	START	END	USED	USED	%
1-1	R 1-1	ROOF	AFFF	60	60.1	45.688	27.188	1001.370	450.000	31.625	30.813	72.000	66.250	551.370	5.750	1.03
1.2	R 2-1	ROOF	AFFF	60	60.2	32.531	8.938	608.333	18.750	30.063	29.313	60.909	53.438	589.583	7.472	1.25
1.3	R 3-1	ROOF	AFFF	60	60.2	45.688	29.313	1001.370	512.963	29.125	28.313	52.500	47.727	488.407 533.333	4.773	0.97
1.5	7	ROOF	AFFF	60	60.1	32.813	12.125	616.667	83.333 474.074	28.219 26.500	27.563 25.813	47.045 36.154	42.694 31.365	525.926	4.789	0.90
1-6	14	ROOF	AFFF	60	60.1	45.625 43.438	28.000 25.938	935.185	412.963	24.813	23.906	24.169	17.752	522.222	6.417	1.21
1-7	16	ROOF	AFFF	60	60.1	45.531	28.156	997.222	478.704	27.313	26.688	41.155	37.308	518.519	3.847	0.74
1.9	18	ROOF	AFFF	60	60.5	45.625	28.094	1000.000	476.852	26.344	25.688	35.192	30.455	523.148	4.737	0.90
1-10	23	ROOF	AFFF	60	59.9	41.344	24.000	872.115	352.000	25.094	24.125	26.136	19.504	520.115	6.633	1.26
1-11	25	ROOF	AFFF	60	60.0	45.594	28.000	999.074	474.074	25.594	24.750	29.773	23.753	525.000	6.020	1.13
1-12	29	ROOF	AFFF	60	60.0	45.625	28.188	1000.000	479.630	26.156	25.313	33.866	27.727	520.370 571.740	6.139 18.280	3.10
2-1	R 1-3	ROOF	AFFF	. <u>60</u> 60	60.0	45.688 45.625	26.500 26.188	1001.370	429.630 420.370	39.875 30.625	37.063 27.688	130.204 65.000	43.464	579.630	21.536	3.58
2-2	R 2-3	ROOF	AFFF .	- 60	60.2	45.688	26.344	1001.370	425.000	25.938	20.313	32.274	3.183	576.370	29.092	4.80
2.5	1 1	ROOF	AFFF	60	60.1	45.594	28.563	999.074	490.741	37.531	35.313	114.811	99.500	508.333	15.311	2.92
2.6	4/2	ROOF	AFFF	60	60.0	45.625	28.438	1000.000	487.037	34.250	31.813	91.364	73.500	512.963	17.864	3.37
2.7	4/3	ROOF	AFFF	60	60.2	32.875	12.750	618.519	96.154	39.563	37.281	128.669	113.271	522.365	15.397	2.86
2-8	55	ROOF	AFFF	60	65.0	45.625	26.313	1000.000	424.074	37.344	34.781	113.656	95.250	575.926 505.556	18.406	3.10
2-9		ROOF	AFFF	60	60.0	45.438	28.500	739.286	488.889 221.053	39.594 38.531	37.219	128.835	112.886	518.233	16.958	3.17
2-10	13/2	ROOF	AFFF	60	60.2	36.938 45.594	18.625 28.375	999.074	485.185	39.469	37.156	128.168	112.502	513.889	15.667	2.96
2-11	13/2	ROOF	AFFF	<u>60</u>	60.1	45.625	28.406	1000.000	486.111	33.969	31.594	89.321	71.750	513.889	17.571	3.31
2-13	18	ROOF	AFFF	60	60.3	43.344	26.281	932.407	423.148	36.094	33.813	104.792	88.184	509.259	16.608	3.16
2-14	20	ROOF	AFFF	60	60.1	45.625	28.469	1000.000	487.963	39.688	37.375	129.336	113.849	512.037	15.487	2.94
3-1	R 1-6	ROOF	AFFF	.60	60.0	45.688	27.531	1001.370	460.185	39.281	34.156	127.168	90.682	541.185	36.486	6.32
3-2	R 2-6	ROOF	AFFF		60.2	45.688	27.000	1001.370	444.444	31.625	26.156 30.563	72.000 107.000	33.866 64.545	556.925 540.259	38.134 42.455	7.29
3-3	R 3-6	ROOF	AFFF	60	60.0 60.1	45.688 45.500	27.563 28.875	996.296	500.000	36.375	34.625	129.502	94.091	496.296	35.411	6.66
3-5	5	ROOF	AFFF		60.0	43.406	26.688	934.259	435.185	39.219	34.438	126.834	92.727	499.074	34.107	6.40
3.7	8	ROOF	AFFF	60	60.0	43.500	26.969	937.037	443.519	39.312	34.344	127.335	92.045	493.519	35.289	6.67
3-8	13	ROOF	AFFF	60	60.1	45.500	28.875	996.296	500.000	39.188	34.094	126.668	90.227	496.296	36.440	6.84
3.9	15	ROOF	WATER	60	59.8	45.625	29.094	1000.000	506.481	39.563	34.750	128.669	95.000 91.364	493.519	33.669	6.39
3-10	16	ROOF	AFFF	60	60.0 60.3	45.625 45.500	28.906 28.938	1000.000 996.296	500.926	39.375	34.250 34.281	127.668	91.591	494,444	36.077	6.80
3-11	34	ROOF	WATER		60.0	45.625	29.031	1000.000	504.630	39.000	34.500	125.667	93.182	495.370	32.485	6.15
3-13	35	ROOF	WATER	60	60.0	45.625	27.063	1000.000	446.296	39.563	35.000	128.669	97.000	553.704	31.669	5.41
3-14	36	ROOF	AFFF	60	60.2	45.500	28.875	996.296	500.000	39.125	34.688	126.334	94.545	496.296	31.789	6.02
1-1	R8 1-1	ROOF/BUMP	AFFF	. 60	60.3	45.688	18.188	1001.370	211.842	27.969	26.813	45.227	38.077 30.000	789.528 775.054	7.150 8.462	1.08
1.2	RB 2-1	ROOF/BUMP	AFFF	60	60.1 60.0	45.688 45.688	18.875 19.000	1001.370	226.316 228.947	26.875 25.750	25.625 24.375	38.462 30.910	21.251	772.422	9.659	1.24
1.3	RB 3-1	ROOF/BUMP	AFFF	. 60 .	60.0	45.500	18.250	996.296	213.158	28.813	27.875	50.938	44.618	783.138	6.319	0.80
1-6	4	ROOF/BUMP	AFFF	60	60.1	45.594	18.219	999.074	212.500	27.906	27.000	44.811	39.231	786.574	5.580	0.70
1-7	5	ROOF/BUMP	AFFF	60	60.0	45.563	17.875	998.148	205.263	27.000	26.063	39.231	33.184	792.885	6.047	0.76
1-8	7	ROOF/BUMP	AFFF	60	60.0	45.625	18.000	1000.000	207.895	28.250	27.375	47.273	41.539	792.105	5.733	0.72
1.9	8	ROOF/BUMP	AFFF	. 60	60.0	45.625	18.000	1 000.0 00 991.667	207.895	27.375 25.375	26.469	41.539 28.182	35.962 18.503	792.105 789.035	5.578 9.679	1.21
1-10	30 31	ROOF/BUMP	AFFF	60	60.1	45.344 44.594	17.750	969.444	181.081	26.125	24.969	33.639	25.227	788.363	8.412	1.06
1-12	32	ROOF/BUMP	AFFF	60	60.0	44.969	17.500	980.556	197.297	24.906	23.469	24.795	14.607	783.258	10.188	1.28
2-1	RB 1-3	ROOF/BUMP	AFFF	60	60.1	45.625	16.438	1000.000	174.324	35.313	31.156	99.500	68.542	825.676	30.958	3.61
2-2	RB 2-3	ROOF/BUMP	AFFF	60	60 .0	45.688	16.438	1001.370	174.324	33.563	29.625	86.365	55.000	827.046	31.365	3.65
2-3	RB 3-3	ROOF/BUMP	AFFF	60	60.1	45.250	17.875	988.889	205.263	27.750	22.563	43.849 105.500	10.790	783.626 777.485	33.059 24.875	3.10
2-5	9	ROOF/BUMP	AFFF		60.0	45.531 45.500	19.094	997.222	219.737 230.921	36.188	32.719 32.875	106.250	80.625 81.667	765.375	24.583	3.11
2-6	10/2	ROOF/BUMP	AFFF	60 60	60.3 60.0	45.500	18.813	996.296	225.000	39.531	36.031	128.502	104.375	771.296	24.127	3.03
2-8	11/2	ROOF/BUMP	AFFF	. 60	60.1	45.594	19.031	999.074	229.605	38.656	35.250	123.542	99.000	769.469	24.542	3.09
2-9	11/3	ROOF/BUMP	AFFF	60	60.2	45.594	18.625	999.074	221.053	36.031	32.656	104.375	80.208	778.021	24.167	3.01
2-10	12/2	ROOF/BUMP	AFFF	60	60 .0	45.594	18.625	999.074	221.053	35.281	31.813	99.250	73.500	778.021	25.750	3.20
2-11	12/3	ROOF/BUMP	AFFF	60	59.9	45.594	18.844	999.074	225.658	37.406	34.031	114.041	89.776 82.500	773.416 768.421	24.265 24.500	3.04
2-12	22	ROOF/BUMP	AFFF	. 60	60.0 60.0	45.625 45.625	19.125	1000.000	231.579 226.316	36.375 33.031	33.000 29.563	107.000 82.708	54.688	773.684	28.021	3.50
2-13	23 24	ROOF/BUMP	AFFF	. 60 60	60.1	45.313	18.844	990.741	225.658	29.563	26.094	54.688	33.412	765.083	21.276	2.71
3-1	RB 1-0	ROOF/BUMP	AFFF	60	60.3	45.000	15.313	981.481	150.000	30.438	21.438	63.636	6.429	831.481	57.208	6.44
3-2	RB 2-6	ROOF/BUMP	AFFF	όO	60.2	45.688	16.500	1001.370	175.676	37.500	29.938	114.618	60.000	825.694	54.618	6.01
3-3	RB 3-6	ROOF/BUMP	AFFF	60	60.1	45.625	19.500	1000.000	239.474	31.313	22.938	69.583	12.369	760.526	57.214	7.00
3-5	10	ROOF/BUMP	AFFF	Oc.	59 .9	45.53!	19.906	997.222	248.026	39.375	32.344	127.668	. 77.750 77.750	7 49 .196 7 50 .000	49.918 50.585	6.25 6.32
3-6	11	ROOF/BUMP	AFFF	50 50	60.0 60.0	45.625 45.469	20.000 19.906	1 000 .000 995.370	250.000 248.026	39.500 39.500	32.344 32.343	128.335 128.335	77.750	747.344	50.563	6.34
3-7 3-8	12	ROOF/BUMP	AFFF WATER	ა0 ა0	50.1	45.625	19.563	:000.000	240.789	39.563	32.750	128.669	80.833	759.211	47.835	5.93
3.9	14	ROOF/BUMP	WATER	50	ó0. i	45.525	9.813	1000.000	246.053	39.688	33.000	129.336	32.500	753.947	46.836	5.85
3-10	[:] 5	ROOF/BUMP	WATER	50	50.2	45 .525	19.562	:000.000	240.779	* 39.625	32.938	129.002	82.083	759.221	46.919	5.82
3.11	22	ROOF/BUMP	AFFF	50	50 .0	45.625	20.188	1000.000	254.286	39.500	32.313	128.335	77.500	745.714	50.835	6.38
3-12	23	ROOF/BUMP	AFFF	50	50.1	45.525	20.125	1000.000	252.857	36.000	29.563	104.167 58.005	54.688 18.253	747.143 5 36 .296	49.479 39.752	6.21 5.88
3-13	24	ROOF/BUMP	AFFF	50	50 .ບ	45 .500	24.250	796.296	360.000	29.813	23.969	30.003	, 0.200	330.270	37.732	.5.00



ND RESULTS

		TANK				CALC.	TARGET		FLOW				D CYLINDER
	CHES	-	LONS	WATER	AFFF	RATIO	RATIO	ERROR	RATE	AMB.	TEST		CHES
TART	END	START	END	USED	5.750	1.03	%	0.03	(GPM) 556.2	TEMP 56	DATE 18-Dec-92	START	END
.625 0.063	30.813 29.313	72.000 60.909	66.250 53.438	551.370 589.583	7.472	1.25		0.25	595.1	58	18-Dec-92		
2.125	28.313	52.500	47.727	488.407	4.773	0.97	ī	-0.03	491.5 .	65	18-Dec-92		
3.219	27.563	47.045	42.694	533.333	4.351	0.81	1	-0.19	536.8	89	23-Jun-93		
.500	25.813	36.154	31.365	525.926	4.789	0.90	1	-0.10	529.8	80	24-Jun-93		
1.813	23.906	24.169	17.752	522.222	6.417	1.21		0.21	526.9	81	24-Jun-93		
.313	26.688 25.688	41.155 35.192	37.308	518.519 523.148	3.847	0.74		-0.26 -0.10	521.5 523.5	82 83	24-Jun-93 24-Jun-93		
.094	24.125	26.136	30.455 19.504	520.115	6.633	1.26	- i	0.26	527.6	83	24-Jun-93		
.594	24.750	29.773	23.753	525.000	6.020	1.13	1	0.13	531.0	84	24-Jun-93		
.156	25.313	33.866	27.727	520.370	6.139	1.17	ì	0.17	526.5	86	20-May-93		
.875	37.063	130.204	111.924	571.740	18.280	3.10	3	0.03	590.0	74	16-Dec-92		
.625	27.688	65.000	43.464	579.630	21.536	3.58	3	0.19	599.2	74	16-Dec-92		
.938	20.313	32.274	3.183	576.370	29.092	4.80	3	0.60	603.5	69	17-Dec-92		
.531 1.250	35.313	91.364	73.500	508.333	15.311	3.37	3	-0.03 0.12	522.8 530.8	_85 85	22-Jun-93 22-Jun-93		
.563	37.281	128.669	113.271	522.365	15.397	2.86	3	-0.05	536.0	82	23-Jun-93	0.002	0.002
.344	34.781	113.656	95.250	575.926	18.406	3.10	3	0.03	548.6	82	23-Jun-93		
.594	37.219	128.835	112.886	505.556	15.949	3.06	3	0.02	521.5	86	22-Jun-93		
1.531	36.219	122.708	105.750	518.233	16.958	3.17	3	0.06	533.4	83_	23-Jun-93		
.469	37.156	128.168	112.502	513.889	15.667	2.96	3	-0.01	528.7 530.6	<u>83</u> 86	22-Jun-93 23-Jun-93		
.969	31.594	89.321 104.792	71.750 88.184	513.889	17.571	3.31	3	0.10	523.3	82	22-Jun-93	with the second section of the second	
.688	37.375	129.336	113.849	512.037	15.487	2.94	3	-0.02	526.6	82	22-Jun-93		
.281	34.156	127.168	90.682	541.185	36.486	6.32	٥	0.05	577.7	72	17-Dec-92		
.625	26.156	72.000	33.866	556.925	38.134	6.41	6	0.07	593.1	72	17-Dec-92		
.375	30.563	107.000	64.545	540.259	42.455	7.29	6	0.21	582.7	72	17-Dec-92		
1.719	34.625	129.502	94.091	496.296 499.074	35.411 34.107	6.66	6	0.11	530.8 533.2	78 83	25-Jun-93 25-Jun-93		
.312	34.438 34.344	126.834	92.727 92.045	493.519	35.289	6.67	6	0.11	528.8	83	25-Jun-93		
.188	34.094	126.668	90.227	496.296	36.440	6.84	6	0.14	531.9	84	25-Jun-93		
.563	34.750	128.669	95.000	493.519	33.669	6.39	6	0.06	529.0	70	10-Mar-93	35.250	35.250
.375	34.250	127.668	91.364	499.074	36.304	6.78	6	0.13	535.4	84	25-Jun-93		
.375	34.281	127.668	91.591	494.444	36.077 32.485	6.80	6	0.13	527.9 527.9	84 81	25-Jun-93 19-May-93	28.688	28.688
.563	34.500 35.000	125.667 128.669	97.000	553.704	31.669	5.41	6	-0.10	585.4	81	19-May-93	28.688	28.688
.125	34.688	126.334	94.545	496.296	31.789	6.02	6	0.00	526.3	80	19-May-93	,	
.969	26.813	45.227	38.077	789.528	7.150	0.90	1	-0.10	792.7	66	18-Dec-92		
.875	25.625	38.462	30.000	775.054	8.462	1.08	!	0.08	782.2	67	18-Dec-92	618 1179 W/94	hanner seller some vir vir vir vir vir den
.750	24.375	30.910	21.251 44.618	772.422 783.138	9.659 6.319	0.80	1	-0.20	782.1 789.5	- 68 - 78	18-Dec-92 24-Jun-93		
.813 .906	27.875 27.000	50.938	39.231	786.574	5.580	0.70		-0.30	790.8	78	24-Jun-93		
.000	26.063	39.231	33.184	792.885	6.047	0.76	1	-0.24	798.9	79	24-Jun-93		
250	27.375	47.273	41.539	792.105	5.733	0.72	1	-0.28	797.8	79	24-Jun-93		
.375	26.469	41.539	35.962	792.105	5.578	0.70	!	-0.30	797.7	79	24-Jun-93		
375	24.000 24.969	28.182	18.503 25.227	789.035 788.363	9.679 8.412	1.21	1	0.21	797.4 795.4	86 87	24-Jun-93 24-Jun-93		
.125 .906	23.469	33.639 24.795	14.607	783.258	10.188	1.28		0.28	793.4	87	24-Jun-93		
.313	31.156	99.500	68.542	825.076	30.958	3.61	3	0.20	855.2	74	16-Dec-92		
563	29.625	86.365	55.000	827.046	31.365	3.65	3	0.22	858.4	69	17-Dec-92		
750	22.563	43.849	10.790	783.626	33.059	4.05	3	0.35	815.3	69	17-Dec-92		
188	32.719	105.500	80.625	777.485	24.875	3.10	3	0.03	802.4 786.0	83_ 86	23-Jun-93 22-Jun-93		
.281 .531	32.875 36.031	106.250 128.502	81.667 104.375	765.375 771.296	24.583	3.11	3 -	0.01	795.4	83	23-Jun-93		
656	35.250	123.542	99.000	769.469	24.542	3.09	3	0.03	792.7	84	22-Jun-93		
031	32.656	104.375	80.208	778.021	24.167	3.01	3	0.00	799.5	84	23-Jun-93		
281	31.813	99.250	73.500	778.021	25.750	3.20	3	0.07	803.8	84	22-Jun-93		
406	34.031	114.041	89.776	773.416	24.265	3.04		0.01	799.0	84	23-Jun-93		
375 031	33.000 29.563	107.000 82.708	82.500 54.688	768.421 773.684	24.500 28.021	3.50	<mark>3</mark>	0.03	792.9 801.7	82 82	22-Jun-93 22-Jun-93		
563	26.094	54.688	33.412	765.083	21.276	2.71	3	-0.10	785.1	82	22-Jun-93		
438	21.438	63.636	6.429	831.481	57.208	6.44	6	0.07	884.3	50	18-Dec-92	-	
5 00	29.938	114.618	60.000	825.694	54.618	6.01	<u> </u>	0.00	877.4	50	18-Dec-92		
313	22.938	69.583	12.369	760.526	57.214	7.00	. 6	0.17	816.4	50	18-Dec-92		
375	32.344	127.668	77.750	749,196	19.918	6.25	5 .	0.04	800.4	83	25-Jun-93 25-Jun-93		-
5 00 5 00	32.344 32.343	128.335 128.335	77.750 77.744	750.000 747.344	50.585 50.591	6.32 6.34	ó .	0.05 0.06	800.6 797.9	84 84	25-Jun-93		
563	32.750	128.669	80.833	759.211	47.835	5.93	0	-0.01	805.7	78	19-May-93		
688	33.000	129.336	32.500	753.947	46.836	5.85	5	-0.03	799.5		19-May-93		
625	32.938	129.002	82.083	759.221	46.919	5.82	ń	-0.03	303.5	78	19-Mav-93		
500	32.313	128.335	77.500	745.714	50.835	6.38	5	0.06	796.5	86	25-Jun-93		
000	29.563	104.157	54.688	747,143	49.479	6.21	٥	0.04	796.6	86 84	25-Jun-93		
813	23.969	58.005	18.253	536.296	39.752	5.88	5	-0.02	811.3	84	25-Jun-93		



APPENDIX A NORDIC MARK IIA EVALUATION MATRIX AND RESULTS

NO	FIGURE			Τ	PLANNED	ACTUAL		WATE	RTANK			AFF	TANK				CA
1	GRAPH	TEST		AFFF	DISPENSING	DISPENSING	INC	CHES	GAL	LONS	INC	CHES	GAL	LLONS	4	1	RA.
12 12 MUMPÉR AFFF 00	NO.										-				_		با
1-3 1.5 MARPÉR AFFF CO 60.0 25.93 11.250 71.074 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 73.05 74.01 74.05 74.01 74.05 74.01 74.05 74.01 74.05 74.01 74.05 74.0						and the same of th			the state and the								0.
1-0 ENAMPTE AFFE 60 60.0 25.000 17.972 17.4010 190.0						WAR I COMMON TO THE PARTY OF TH											1.
10 S. BIAMPÉE AFF 60 600 2598 14.596 342.761 329.00 21.808 22.818 27.208 21.815 21.800 21.800 21.80																	1.
14 17 SUMPER AFF 00									412.963					13.422	-	4.330	1.
1-9	1-7	17	BUMPER														0.
1-10								***************************************									
1-11 27 SUMPER AFF																	$-\frac{1}{1}$
22 81-3 SUMPER AFFF 60 60.3 56.88 12.999 42.0370 100.659 22.888 20.313 43.644 50.000 279.549 40.440 22.888 23.888 24.878 60.000 36.549 50.000 279.549 40.000 279.549 40.0000					F 800 F 71 M 5					and the second or second							1.
22 8.23 BUMPER AFFF O O.01 55.568 55.675 O.01 370 701.786 36.725 34.875 35.500 50.000 50.000 34.75 34.875 35.500 50.000 34.75 34.875 35.500 50.000 34.75 34.875 35.500 50.000 34.75 34.875 35.500 50.000 34.875 34.875 35.500 50.000 34.875 34.875 35.500 50.000 34.875 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 34.875 35.500 35.500 34.875 34.875 35.500 34.875																	2.
23 S. S. SUMPER AFFF O. O. 20.2 S.					· · · · · · · · · · · · · · · · · · ·											9.000	2.
2.20 3			BUMPER	AFFF	60	60.2	35.625	25.188	701.786	390.000	34.875			85.910			3.
22 5	2-5		BUMPER						# 1000FF 1 10 1					-			2.
24				de la marco de la marco de la composición dela composición dela composición dela composición dela composición de la composición dela composición de la composición dela composición del composición dela composición dela composición del composición dela com													2.
20 172 BILMPEP AFF 00 60.1 52.50 53.93 50.000 797.26 53.93 38.51 12.820 103.750 52.505 71.95																	2.
2-10 17/3 SUMPER AFF 00 60.0 26.75 18.31 48.15 20.071 17.70 17				an eller 1 m					A SECTION 1 STREET	****** ** ****** * *							2.
1472 BUMPÉR AFFF 60 600 28.375 18.351 48.185 219.074 37.156 36.004 112.500 41.772 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 26.112 77.10 14.172 27.172 14.172 1					tige on the generalization that the												2.
2013 17				AFFF	60	60.0	28.375	18.531	485.185	219.074							2.
23.14 19		·			· · · · · · · · · · · · · · · · · · ·												2.
231 21 SUMPÉR AFF 00 00.5 28.407 18.688 487 90.3 222.368 37.375 31.8847 107.000 265.575 5.849 32.4 34.4044 34.724 34.675 34.8 34																	2.
11 10 BUMPÉR AFFF SO SO 27 27 53 15 500 40 18 15 500 20 27 27 27 27 27 27		·															2.
3-2 B 2-0 BUMPER AFFE 60 001 27000 53.13																	5.
3-5 2 SUMPER AFFF 60 60.0 27.503 15.313 461.11 150.000 20.503 27.675 45.555 44.616 311.111 19.727 3-5 6 SUMPER AFFF 60 60.0 26.888 16.750 45.155 18.108 34.842 34.225 32.405 94.079 77.550 25.4104 16.227 3-7 3-7 8 SUMPER AFFF 60 60.0 26.888 16.750 45.155 18.108 34.843 32.168 97.227 76.500 254.104 16.227 3-8 9 SUMPER AFFF 60 60.0 26.999 17.063 445.151 167.538 34.34 32.094 27.050 257.785 16.932 3-9 10 SUMPER AFFF 60 60.0 26.999 17.063 445.151 167.538 34.34 32.094 27.054 57.550 257.596 17.550 37.996 3-9 10 12 SUMPER WATER 60 60.0 26.999 17.063 445.151 167.538 34.34 32.094 27.550 267.799 17.550 37.999 17.550 37.599 3					A C C CONTRACT C C C			4 manufacture							294.444	26.724	8.
3.7 S	3-3	B 3-6	BUMPER	AFFF	60	60.0							·				6.0
33 9 BUMPER AFF 60 60.1 97.031 19.375 504.030 23.686 3.150 33.165 70.295 207.788 16.932 38 8 BUMPER AFF 60 60.0 28.987 17.985 16.955 205.086 16.295 17.9125 300.000 23.585 37.000 9.205 7.575 205.086 16.295 17.9125 300.000 23.585 37.000 9.205 7.575 205.086 16.295 17.9125 300.000 23.585 37.000 9.205 7.575 205.086 16.295 17.9125 300.000 23.585 37.000 9.205 7.575 205.086 16.295 17.9125 300.000 23.585 37.000 9.205 7.575 205.000 23.585 17.000 9.205 7.575 205.000 23.585 17.000 9.205 7.575 17.500 9.205 7.500 9.205				A THE R PROPERTY OF THE										****			5.4
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3-0 10																	5.
3-11 15 8UMPER AFFF 60 9.01 28,906 19,086 500,092 243,421 34,250 32,156 91,364 76,229 25,7505 15,114 11, 11-11 14, 1																17.500	6.
3-12 77				A													6.2
313 20 BUMPER AFFF 60 60 29,093 19,719 501,852 24,079 34,281 32,000 19,191 75,000 25,773 16,591 31,141 11 11 11 14 14 14 14																	5.5
3-14 28 BUMPER AFFF 60 59.0 30.285 31.219 813.842 589.444 23.875 20.000 17.502 24.25 24.40.17 5.077 1.1 1.1 HANDINE AFFF 60 60.1 37.503 35.004 757.407 685.577 30.186 33.182 61.818 71.830 3.84 30.313 62.955 62.727 72.773 0.222 31.1 3.1 HANDINE AFFF 60 60.0 35.004 37.503 35.004 37.503 30.503 30.188 30.003 31.818 60.909 77.244 0.909 31.518 3.1 4.3 3.3 3.4 3.0 3.1 4.3 3.3 3.4 3.0 3.3 3.4 3.0 3.3 3.4 3.0 3.3 3.0 3						and the second second second second											6.0
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2-1 H-3 HANDLINE AFFF 120 120.1 15.250 8.188 148.684 3.750 35.813 35.188 102.917 98.500 144.934 4.417 2.22 H-2.3 HANDLINE AFFF 60 60.2 13.250 9.625 106.579 32.500 30.813 30.500 66.250 64.091 74.079 2.159 7.23 14.33 HANDLINE AFFF 60 60.2 12.969 9.344 100.658 26.875 26.313 26.000 35.000 32.729 73.783 2.271 2.5 1. HANDLINE AFFF 60 60.0 45.625 43.438 100.000 935.185 39.719 39.719 129.502 129.502 64.815 2.178 2.7 8 HANDLINE AFFF 60 60.1 43.437 41.438 935.185 875.000 39.719 39.719 129.502 129.502 64.815 1.987 2.7 8 HANDLINE AFFF 60 60.0 15.875 13.000 162.162 101.316 36.218 105.750 105.750 61.522 16.36 2.8 9 HANDLINE AFFF 60 60.0 15.875 13.000 162.162 101.316 36.218 105.750 105.750 60.844 1.657 2.9 1.657 2.10 1.6																	2.4
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2-6 1 HANDLINE AFFF 60 60.0 45.625 43.438 1000.000 935.185 39.719 39.719 129.502 129.502 64.815 2.178 2.2-6 2 HANDLINE AFFF 60 60.1 18.750 15.875 223.684 162.162 36.219 105.750 1	2-3		HANDLINE	AFFF	60		12.969	9.344	100.658	26.875	26.313			-			5.0
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3.3 H 3.6 HANDLINE AFFF 60 60.0 40.938 38.500 859.615 785.185 30.969 30.438 67.292 63.636 74.430 3.655 4 6 7.500 78.250 7															neter our Advancer	AM TO 1 T 1	4.9
3.5 3 HANDLINE AFFF 60 60.1 19.688 16.875 243.421 183.784 32.406 32.406 78.250 78.250 59.637 3.357 8 3.6 4/5 HANDLINE AFFF 60 59.9 45.531 43.406 977.222 934.259 39.594 39.219 128.835 126.834 62.963 5.380 7 3.7 1/1 HANDLINE WATER 60 60.0 45.281 43.219 989.815 928.704 23.813 23.813 17.002 17.002 61.111 3.464 5 3.9 14 HANDLINE AFFF 60 60.1 45.594 43.500 999.074 937.037 39.500 39.313 128.335 127.335 62.037 4.475 63 63.9 14 HANDLINE AFFF 60 60.2 28.875 26.844 500.000 439.815 34.094 34.063 90.227 90.000 60.185 33.10 18 HANDLINE AFFF 60 60.1 19.688 16.750 243.421 181.081 32.156 32.094 76.250 75.750 52.340 3.836 53.11 21 HANDLINE AFFF 60 60.2 19.719 16.906 244.079 184.459 32.000 31.938 75.000 74.500 59.619 3.879 63.12 25 HANDLINE AFFF 50 60.2 19.719 16.906 244.079 184.459 32.000 31.938 75.000 74.500 59.619 3.879 63.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.11 51.11			The second of th														4.
3-7 4/1 HANDLINE WATER 60 60.0 45.281 43.219 989.815 928.704 23.813 23.813 17.002 17.002 61.111 3.464 53.8 7 HANDLINE AFFF 60 60.1 45.594 43.500 999.074 937.037 39.500 39.313 128.335 127.335 62.037 4.475 63.39 14 HANDLINE AFFF 60 60.2 28.875 26.844 500.000 439.815 34.094 34.063 90.227 90.000 50.185 3.468 53.10 18 HANDLINE AFFF 60 50.1 19.688 16.750 243.421 181.081 32.156 32.094 76.250 75.750 52.340 3.836 53.11 21 HANDLINE AFFF 50 60.2 19.719 16.906 244.079 184.459 32.000 31.938 75.000 74.500 59.619 3.879 63.12 25 HANDLINE AFFF 50 50.0 45.625 43.469 1000.000 936.111 23.906 23.813 17.752 17.002 63.889 4.161 63.313 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.415		3	HANDLINE	AFFF		60.1	19.688	16.875									5
3.8 7 HANDLINE AFFF 60 60.1 45.594 43.500 999.074 937.037 39.500 39.313 128.335 127.335 62.037 4.475 63.39 14 HANDLINE AFFF 60 60.2 28.875 26.844 500.000 439.815 34.094 34.063 90.227 90.000 50.185 3.468 53.10 18 HANDLINE AFFF 60 50.1 19.688 16.750 243.421 181.081 32.156 32.094 76.250 75.750 52.340 3.836 53.11 21 HANDLINE AFFF 50 60.2 19.719 16.906 244.079 184.459 32.000 31.938 75.000 74.500 59.619 3.879 63.12 25 HANDLINE AFFF 50 50.0 45.625 43.469 1000.000 936.111 23.906 23.813 17.752 17.002 63.889 4.161 63.13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.11 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 53.11 51.502 17.502 51.111 3.241 53.2	,																7.3
3-9 14 HANDLINE AFFF 60 60.2 28.875 26.844 500.000 439.815 34.094 34.063 90.227 90.000 50.185 3.468 5 3-10 18 HANDLINE AFFF 60 50.1 19.688 16.750 243.421 181.081 32.156 32.094 76.250, 75.750 52.340 3.836 5 3-11 21 HANDLINE AFFF 50 60.2 19.719 16.906 244.079 184.459 32.000 31.938 75.000 74.500 59.619 3.879 6 3-12 25 HANDLINE AFFF 50 50.0 45.625 43.469 1000.000 936.111 23.906 23.813 17.752 17.002 63.889 4.161 63.313 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 5	- 1																5.
3-10 18 HANDLINE AFFF 60 60.1 19.688 16.750 243.421 181.081 32.156 32.094 76.250. 75.750 52.340 3.836 5.53																	5. 5.
3-11 21 HANDLINE AFFF 50 60.2 19.719 16.906 244.079 184.459 32.000 31.938 75.000 74.500 59.619 3.879 60.00 25 HANDLINE AFFF 50 60.0 45.625 43.469 1000.000 936.111 23.906 23.813 17.752 17.002 63.889 4.161 60.000 20.00000 20.0000 20.0000 20.0000 20.0000 20.0000 20	- 1																5.8
3-12 25 HANDLINE AFFF 50 50.0 45.625 43.469 1000.000 936.111 23.906 23.813 17.752 17.002 63.889 4.161 6 3-13 26 HANDLINE AFFF 50 60.1 43.469 41.438 936.111 975.000 23.875 23.875 17.502 17.502 51.111 3.241 5																	5.
													17.752	17.002			Ó.
3-14 27 HANDLINE AFFF 60 60 41.438 39.438 875.000 813.462 23.875 23.875 17.502 17.502 61.538 - 3.071 4																	5.0
	3-14	27	HANDLINE	AFFF	50	ó0 !	41.438	39.438	375.000	813.462	23.875	23.875	17.502	17.502	61.538 -	3.071	4.7



AND RESULTS

	AFFF TANK		1		CALC.	TARGET		FLOW		1	AFEE NOR	D CYLINDER	
INC	CHES		LLONS	WATER	AFFF	RATIO	RATIO	ERROR	RATE	AMB.	TEST		CHES
START	END	START	END	USED	USED	%	%	%	(GPM)	TEMP	DATE	START	END
30.813	30.344	66.250	62.955	311.842	3.295	1.05	1	0.05	314.6	56	18-Dec-92		
29.313	29.031	53.438	52.031	260.256	1.406	0.54		-0.46	261.7	65	18-Dec-92		
24.438 25.813	23.969 25.406	21.668 31.365	18.253 28.409	306.384 267.495	3.415 2.956	1.10		0.10	309.8 270.5	68 80	18-Dec-92 24-Jun-93		
23.906	23.188	17.752	13.422	270.200	4.330	1.58	i	0.58	274.5	81	24-Jun-93		· · · · · · ·
26.688	26.344	37.308	35.192	270.809	2.115	0.78	1	-0.22	272.9	82	24-Jun-93		
25.688	25.219	30.455	27.045	270.273	3.409	1.25		0.25	273.2	83	24-Jun-93		
24.125 26.906	23.500	19.504	14.739	267.385	4.765 2.692	1.75		0.75	272.1	83	24-Jun-93 24-Jun-93		-
26.469	26.469 26.063	38.654	35.962 33.184	266.071 261.706	2.777	1.05		0.05	264.5	86	24-Jun-93		
27.688	26.313	43.464	35.000	319.712	8.464	2.58	3	-0.14	326.5	74	16-Dec-92		
36.125	34.875	105.000	96.000	299.584	9.000	2.92	3	-0.03	307.0	69	17-Dec-92		
34.875	33.500	96.000	85.910	311.786	10.090	3.13	3	0.04	320.8	69	17-Dec-92		
35.313 39.563	34.344	99.500 128.669	92.045 128.669	256.481	7.451	2.76	3	-0.08 -0.02	269.5 263.8	85 82	22-Jun-93 23-Jun-93	22.813	0.016
31.813	30.813	73.500	66.250	263.353	7.250	2.68	3	-0.11	270.6	85	22-Jun-93		0.51.5
34.781	33.719	95.250	87.502	263.939	7.748	2.85	3	-0.05	271.7	82	20-May-93		
37.219	36.219	112.886	105.750	265.205	7.136	2.62	3	-0.13	271.9	86	22-Jun-93		
39.531 37.156	38.531 36.094	128.502	122.708	260.714 266.112	7.710	2.17	3	-0.28 -0.06	266.5 273.8	83 83	23-Jun-93 22-Jun-93		
11.594	30.563	71.750	64.545	265.058	7.205	2.65	3	-0.12	272.3	86	23-Jun-93		
0.562	30.562	64.542	64.542	132.898	4.006	2.93	3	-0.02	269.3	86	23-Jun-93	24.750	12.969
3.813	32.556	88.184	80.208	264.357	7.976	2.93	3	-0.02	272.3	82	22-Jun-93		
17.375 14.156	36.375 31.525	90.682	72.000	265.595 306.131	6.849 18.682	2.51 5.75	6	-0.16	270.2 323.7	82 72	22-Jun-93 17-Dec-92		
6.156	21.625	33.866	7.143	294.444	26.724	8.32	6	0.39	320.6	72	17-Dec-92		
0.563	27.875	64.545	44.618	311.111	19.927	6.02	ó	0.00	331.0	72	17-Dec-92		
4.625	32.406	94.091	78.250	256.579	15.841	5.81	6	-0.03	272.0	82	25-Jun-93		
4.438 4.500	32.188 32.156	92.727	76.500 76.250	254.104 267.788	16.227	6.00 5.95	6	-0.00	270.3 284.2	83	25-Jun-93 19-May-93		
4.344	32.094	92.045	75.750	255.681	16.295	5.99	6	0.00	272.0	83	25-Jun-93		
5.000	32.563	97.000	79.500	267.398	17.500	6.14	6	0.02	284.4	81	19-May-93		
4.688	32.219	94.545	76.750	268.421	17.795	6.22	6	0.04	286.2	80	19-May-93		
4.063 4.250	31.813	90.000	73.500 76.250	256.031	16.500	6.05 5.54	6	-0.08	272.5 272.6	84	25-Jun-93 25-Jun-93		
4.281	32.000	91.591	75.000	257.773	16.591	6.05	6	0.01	273.9	84	25-Jun-93		
3.875	20.000	17.502	2.425	244.017	15.077	5.82	ó	-0.03	260.8	87	25-Jun-93		
0.344 0.375	30.313	62.955	62.727	72.773	1.364	0.31		-0.69 0.86	72.9 73.1	.56	18-Dec-92		
0.3/3	30.188	63.182	61.818	77.244	0.909	1.16	<u></u>	0.16	78.2	58	18-Dec-92		
8.531	28.531	49.318	49.318	63.158	0.850	1.33	1	0.33	64.0	87	23-Jun-93	30.000	27.500
8.594	28.594	49.773	49.773	62.037	0.701	1.12	!	0.12	62.6	89	23-Jun-93	27.625	25.563
8.594 4.813	28.594	49.773 24.169	<u>49.773</u> <u>24.169</u>	61.075 64.815	0.701	2.08 1.07		0.07	65.5	89 81	23-Jun-93 24-Jun-93	25.563 29.625	21.750 27.563
5.094	25.094	26.136	26.136	62.802	1.594	2.47	1	1.47	64.4	83	24-Jun-93	27.625	22.938
5.094	25.094	26.136	26.136	64.815	0.691	1.05	1	0.05	65.4	83	24-Jun-93	22.875	20.844
5.093	25.094	26.136	26.136	61.218	1.519	2.42		1.42	62.5	83	24-Jun-93	20.844 16.313	16.375
6.063 5.813	26.062 35.188	33.184 102.917	33.180 98.500	62.963	1.562 4.417	2.42	3	-0.01	64.5 74.6	86 74	24-Jun-93 16-Dec-92	10.515	11.717
0.813	30.500	66.250	64.091	74.079	2.159	2.83	3	-0.06	76.0	74	16-Dec-92		
6.313	26.000	35.000	32.729	73.783	2.271	5.38	3	0.79	74.6	74	16-Dec-92		
9.719	39.719 39.719	129.502	129.502	64.815	2.178	3.25	3	0.08	67.0	82	23-Jun-93	35.063 28.656	28.656 22.813
9.719 6.219	36.219	129.502 105.750	105.750	60.185	1.636	3.20 2.59	3	0.07 -0.14	62.1	82 86	23-Jun-93 22-Jun-93	35.313	30.500
5.218	36.218	105.750	105.750	60.846	1.657	2.65	3	-0.12	62.5	86	22-Jun-93	30.500	25.625
5.094	36.094	104.792	104.792	58.944	1.562	2.58	3	-0.14	60.5	83	22-Jun-93	34.344	29.750
0.563 5.094	30.563 36.094	64.545 104.792	64.545 104.792	62.963	1.732	2.68	3	-0.11 -0.18	62.3	86 83	23-Jun-93 22-Jun-93	34.844 29.750	29.750 25.250
0.563	30.563	64.545	64.545	61.182	1.700	2.70	<u>3</u>	-0.10	62.8	86	23-Jun-93	29.750	24.750
5.094	36 094	104.792	104.792	64.815	2.029	3.04	3	0.01	66.8	82	22-Jun-93	25.344	19.375
2.063	31.500	75.500	71.000	69.888	4.500	6.05	6	0.01	74.1	50	18-Dec-92		
1.500	30.969	71.000	67.292	71.866	3.708	4.91	. 5 .	0.18	75.6 78.1	50	18-Dec-92 18-Dec-92		-
0.969 2.406	30.438 32.406	67.292 78.250	63.636 78.250	74.430 59.637	3.655 3.357	4.68 5.33	5 5	-0.22 -0.11	78.1 62.9	50 82	25-Jun-93	35.375	25.500
2.594	39 219	128.835	126.834	62.963	5.380	7.87	0	0.31	68.5	83	25-Jun-93	34.688	24.750
1.813	23 513	17.002	17.002	61.111	3.464	5.36	Ó	-0.11	64.6		21-May-93	35.063	24.875
.500	39 313	128.335	127.335	62.037	4.475	5.73	5	0.12	66.4	93	25-Jun-93	35.438	25.219 26.000
1.094 1.156	34 063 32 094	90.227 76.250 ₋	90.000 75.750	50.185 52.340	3.458 3.836	5.45 5.80	5	-0.09 -0.03	63.4 66.1	84 84	25-Jun-93 25-Jun-93	35.531 35.250	25.438
	31 938	75.000	74.500	59.619	3.879	6.11	5	0.02	63.3	84	25-Jun-93	35.313	25.375
.906	23 313	17.752	17.002	53.889	4.161	6.11	5	0.02	68.1	87	25-Jun-93	35.063	25.031
1.875	23 875	17.502	17.502	61.111	3.241	5.04	5	-0.16	64.2	87	25-Jun-93	25.031	15.500
.875	23 875	17 502	17.502	61.538 -	3.071	4.75	5	-0.21	64.5	97	25-Jun-93	15.500	5.469



APPENDIX A NORDIC MARK IIA EVALUATION MATRIX AND RESULTS

		I	T		PLAN	ACTUAL			MEC	CHANICAL M	ETERED DAT	Α
FIGURE				TARGET	DISPENSING	DISPENSING	WATER USAGE - GALS			FOA	M USAGE - G	ALS.
GRAPH NO.	TEST NO.	TURRET	AGENT TANK	RATIO %	TIME (sec)	TIME (sec)	START	STOP	TOTAL	START	STOP	TOTAL USED
1-14	1	ROOF	AFFF	1	60	60.0	28,236	28.733	498	2,380.0	2,385.5	5.4
1-15	2	ROOF	AFFF	1	60	60.1	29.765	30,265	500	2,397.1	2,402.5	5.4
1-16	3	ROOF	AFFF	1	60	60.1	30,265	30.766	501	2,402.5	2.408.2	5.7
1-17	4	ROOF	AFFF	1	60	60.2	30.766	31,279	513	2,408.2	2,413.8	5.6
1-18	5	ROOF	AFFF	1	60	60.2	31.279	31,795	516	2.413.8	2,419.5	5.7
2-16	1	ROOF	AFFF	3	60	60.2	20.742	21.230	488	2,135.4	2,153.4	18.0
2-17	2	ROOF	AFFF	3	60	60.0	22,300	22.802	502	2,174.2	2,190.4	16.2
2-18	3	ROOF	AFFF	3	60	59.9	23.053	23.546	494	2,199.4	2.216.5	17.0
2-19	4	ROOF	AFFF	3	60	60.0	23.546	24.041	495	2,216.5	2,234.1	17.7
2-20	5	ROOF	AFFF	3	60	60.0	24.041	24.536	495	2,234.1	2.251.4	17.3
2-21	1A	ROOF	AFFF	3	60	60.4	18.216	18.735	519	2,045.8	2,063.6	17.8 17.4
2-22	3A	ROOF	AFFF	3	60	60.0	19,740	20.241	501	2,099.1	2,116.5	
3-16	1	ROOF	AFFF	6	60	60.0	40.369	40.845	476 490	2,741.6	2,774.1 2,808.0	32.5 33.9
3-17 3-18	3	ROOF	AFFF	6	60 60	60.1 60.1	40.845 41,335	41,335 41,809	474	2,808.0	2,841.9	33.9
3-19	4	ROOF	AFFF	6	60	59.9	41,809	42.283	474	2,841.9	2,875.1	33.2
3-19	5	ROOF	AFFF	6	60	60.1	42,283	42,758	475	2,875.1	2,907.9	32.8
1-14	16	ROOF/BUMP	AFFF	1	60	60.0	28.993	29.765	772	2,388.4	2,397.1	8.7
1-15	17	ROOF/BUMP	AFFF	1	60	60.1	33,131	33.909	778	2,434.5	2,443.1	8.6
1-16	18	ROOF/BUMP	AFFF	1	60	60.1	33,909	34.683	774	2,443.1	2,452.1	9.0
1-17	19	ROOF/BUMP	AFFF	1	60	60.1	34.687	35,442	755	2,452.1	2,461.5	9.4
1-18	20	ROOF/BUMP	AFFF	1	60	60.2	35.442	36.208	766	2,461.6	2,470.4	8.8
2-16	17	ROOF/BUMP	AFFF	3	60	60.0	25.294	26.037	743	2,279.1	2,305.3	26.2
2-17	18	ROOF/BUMP	AFFF	3	60	59.9	26.037	26.757	720	2,305.3	2,329.8	24.5
2-18	19	ROOF/BUMP	AFFF	3	60	60.0	26,757	27,495	738	2,329.8	2,354.7	24.9
2-19	20	ROOF/BUMP	AFFF	3	60	60.2	27,495	28.236	741	2,354.7	2.380.0	25.3
2-20	2A	ROOF/BUMP	AFFF	3	60	60.0	18,984	19.740	756	2.072.8	2,099.1	26.3
3-15	16	ROOF/BUMP	AFFF	6	60	60.0	36.724	37.462 38.179	738 717	2,498.7 2,550.3	2,550.3 2,598.5	51.6 48.2
3-16 3-17	17	ROOF/BUMP	AFFF	6	60 60	59.9 60.0	37,462 38,179	38,912	733	2,550.5	2,645.7	47.2
3-18	19	ROOF/BUMP	AFFF	6	60	60.1	38,912	39.643	731	2,645.7	2.693.5	47.8
3-19	20	ROOF/BUMP	AFFF	6	60	60.1	39,643	40,369	726	2,693.5	2,741.6	48.1
1-13	6	BUMPER	AFFF	1	60	60.1	28.733	28,993	260	2.385.5	2,388.4	3.0
1-14	7	BUMPER	AFFF	1	60	60.2	31,798	32,071	273	2,419.5	2,422.6	3.1
1-15	8	BUMPER	AFFF	1	60	60.1	32.071	32.333	262	2,422.6	2.425.6	3.0
1-16	9	BUMPER	AFFF	1	60	60.0	32,333	32,596	263	2,425.6	2.428.6	3.0
1-17	10	BUMPER	AFFF	1	60	60.1	32,596	32.863	267	2.428.6	2,431.6	3.0
2-17	7	BUMPER	AFFF	3	60	60.0	22,802	23.053	251	2,190.4	2,199.4	9.0
2-18	8	BUMPER	AFFF	3	60	60.1	24.536	24,791	255	2.251.5	2.260.5	9.0
2-19	9	BUMPER	AFFF	3	60	60.0	24.791 25.042	25.042 25.294	251 253	2,260.5 2,269.7	2,269.7	9.2
2-20	10	BUMPER BUMPER	AFFF	3	60 60	59.9	25,042	25,294	253	2.269.7	2,279.1	8.5
2-22	5	BUMPER	AFFF	3	60	60.1	18.735	18,984	249	2.063.6	2,072.8	9.2
3-16	6	BUMPER	AFFF	6	60	60.0	42,758	43.000	242	2,907.9	2,926.4	18.5
3-17	7	BUMPER	AFFF	6	60	59.9	43.000	43,238	238	2.926.4	2,944.1	17.8
3-18	8	BUMPER	AFFF	6	60	59.9	43,238	43,476	238	2.944.1	2,962.8	18.7
3-19	9	SUMPER	AFFF	6	60	59.9	43.476	43.720	244	2.962.8	2,981.4	18.6
3-20	10	BUMPER	AFFF	6	60	60.0	43.720	43,958	238	2,981.4	3,000.0	18.6
1-14	11	HANDLINE	AFFF	1	60	60.1	32.863	33,131	268	2,431.6	2,434.5	2.9
1-15	12	HANDLINE	AFFF	1	60	60.0	36.208	36.269	61	2,470.4	2,471.6	1.2
1-16	13	HANDLINE	AFFF	1	60	60.1	36.269	36.332	63	2,471.6	2,473.1	1.5
1-17	14	HANDLINE	AFFF	1	60	60.0	36,332	36.388	56	2,473.1	2,474.5	1.4
1-18	15	HANDLINE	AFFF	1	60	59.9	36.388	36.442	54	2.474.5	2,475.8	1.3
2-15	11	HANDLINE	AFFF	3	60	59.8	21.230	21.290	60	2.153.4	2,155.6	2.2
2-16	12	HANDLINE	AFFF	3	60	60.2	21.290	21,346	57	2,155.6	2,158.1	2.5
2-17 2-18	13	HANDLINE	AFFF	3	60	60.1	21,402	21,402	56 59	2,158.1	2,162.5	2.2
2-18	14	HANDLINE HANDLINE	AFFF AFFF	3	60	61.0 59.6	21,402	21,461	57	2,160.3	2.164.7	2.2
3-16	11	HANDLINE	AFFF	6	60	60.0	36,442	36.503	61	2.475.8	2,481.0	5.2
3-16	12	HANDLINE	AFFF	6	60	60.0	36.503	36.555	52	2.475.8	2,481.0	4.4
3-18	13	HANDLINE	AFFF	6	60	60.1	36.555	36.613	58	2,485.4	2,489.7	4.3
3-19	14	HANDLINE	AFFF	6	60	60.1	36,613	36.670	57	2.489.7	2,494.1	4.4
									54	2.494.1	2,498.7	4.6

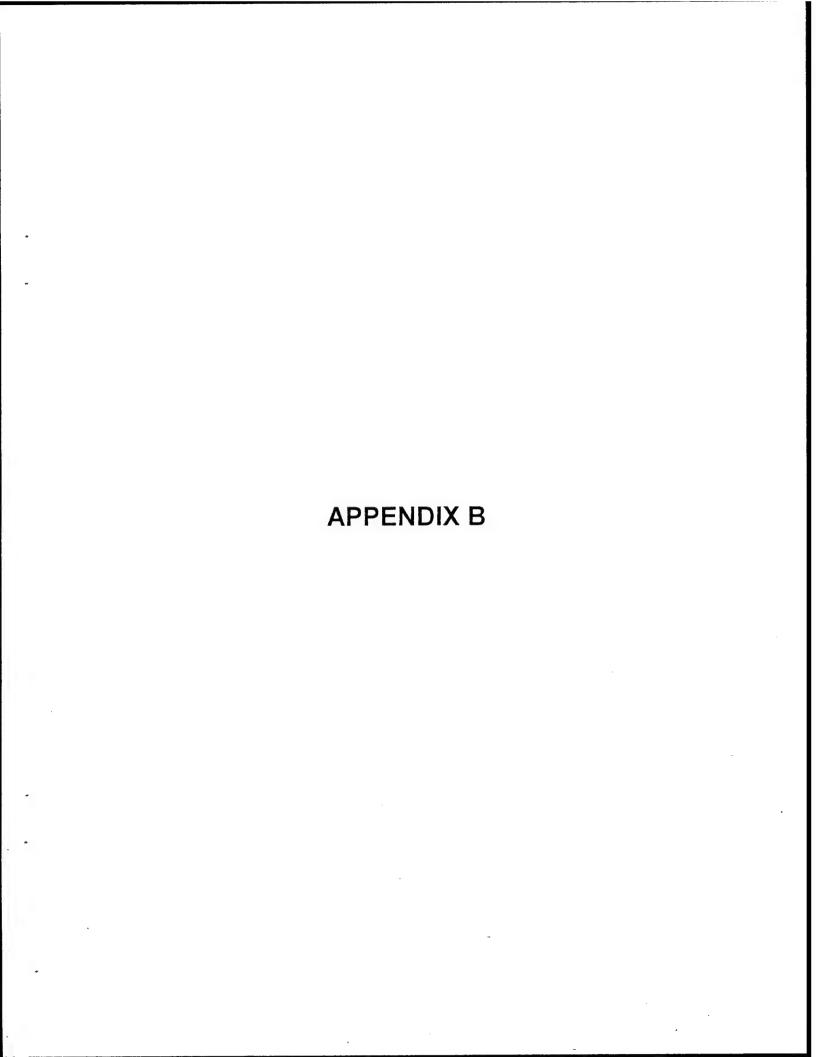


MATRIX AND RESULTS

MAGNETIC FLOW METER DATA

						ELECTRONIC METERED DATA								
MEC		TERED DAT		2112		COLLI	TON USAGE			USAGE - C		CALC		
	FOAI	M USAGE - G		CALC		SOLUI	ION USAGE		FUA	W OSAGE - C	TOTAL	RATIO	ERROR	
AL			TOTAL	RATIO	ERROR	START	STOP	TOTAL	START	STOP	USED	%	%	
D	START	STOP	USED	%	%	START							0.07	
8	2,380.0	2,385.5	5.4	1.08	0.08	57,156.9	57,653.8	503.0	6,166.7	6.171.9	5.38	1.07	0.07	
0	2,397.1	2,402.5	5.4	1.07	0.07	58,671.5	59,172.4	507.0	6,183.7	6,189.2	5.66	1.12	0.12	
1	2,402.5	2.408.2	5.7	1.12	0.12	59,172.4	59,673.9	507.6	6,189.5	6,194.7	5.43	1.07	0.07	
3	2.408.2	2,413.8	5.6	1.08	0.08	59.673.9	60,174.8	507.1	6,195.1	6,200.5	5.48	1.09	0.09	
6	2,413.8	2,419.5	5.7	1.09	0.09	60.174.8	60,680.5	511.8	6,200.7	6.206.1	5.59			
8	2,135.4	2,153.4	18.0	3.56	0.56	49,524.0	50.031.3	513.4	5.921.4	5,938.1	16.91	3.29	0.29	
2	2,174.2	2,190.4	16.2	3.13	0.13	51,074.0	51,579.0	511.1	5.964.0	5,980.5	16.68	3.26	0.24	
4	2,199.4	2.216.5	17.0	3.34	0.34	51,834.3	52,335.3	507.1	5,989.9	6,006.2	16.44	3.24	0.24	
5	2.216.5	2,234.1	17.7	3.44	0.44	52,335.3	52,840.9	511.7	6,006.5	6,023.5	17.20 16.82	3.36	0.31	
5	2.234.1	2,251.4	17.3	3.38	0.38	52.840.9	53,343.0	508.2	6,023.7	6,040.4	18.93	3.47	0.47	
9	2.045.8	2,063.6	17.8	3.32	0.32	46,944.4	47,483.8	545.5	5,831.0	5,849.8	17.17	3.31	0.31	
1	2.099.1	2,116.5	17.4	3.36	0.36	48,495.3	49,007.9	518.7	5.884.2	5.901.2			0.30	
6	2,741.6	2,774.1	32.5	6.39	0.39	69,371.2	69,877.8	512.7	6,518.7	6,550.9	32.32	6.30	0.39	
0	2,774.1	2.808.0	33.9	6.47	0.47	69,887.8	70,393.4	511.7	6,551.0	6,583.6	32.69	6.21	0.39	
4	2.808.0	2.841.9	33.9	6.67	0.67	70.393.4	70,906.0	518.8	6,583.9	6,615.9	32.20		-0.05	
4	2.841.9	2,875.1	33.2	6.55	0.55	70,906.0	71,409.0	509.0	6,616.3	6,646.4	30.31	5.95 6.18	0.18	
5	2,875.1	2.907.9	32.8	6.46	0.46	71,409.0	71,916.4	513.6	6.648.7					
2	2.388.4	2,397.1	8.7	1.11	0.11	57,910.3	58,671.5	767.4	6,175.3	6,183.6	8.43	1.10	0.10	
В	2.434.5	2.443.1	8.6	1.09	0.09	61,959.4	62,727.3	774.1	6,221.7	6,229.9	8.36	1.08	0.08	
4	2,443.1	2,452.1	9.0	1.15	0.15	62,727.3	63,494.5	773.3	6,230.0	6,238.6	8.74	1.13	0.13	
5	2.452.1	2,461.5	9.4	1.23	0.23	63,496.5	64,263.8	767.3	6,239.3	6,248.0	8.79	1.15	0.15	
6	2,461.6	2,470.4	8.8	1.14	0.14	64,263.8	65.034.2	776.5	6,248.3	6,256.5	8.36		0.08	
3	2,279.1	2,305.3	26.2	3.41	0.41	54,116.9	54.878.9	768.0	6,068.0	6,092.7	24.91	3.24	0.24	
9	2,305.3	2,329.8	24.5	3.29	0.29	54.878.9	55.633.2	760.4	6,092.8	6,117.1	24.40	3.21	0.12	
8	2,329.8	2,354.7	24.9	3.26	0.26	55.633.2	56,390.8	767.3	6,117.4	6,141.2	23.96 24.53	3.12	0.12	
1	2,354.7	2,380.0	25.3	3.30	0.30	56,390.8	57,156.9	772.2	6,141.4	6,165.8 5,884.1	24.53	3.26	0.16	
6	2,072.8	2,099.1	26.3	3.36	0.36	47,737.9	48,495.3	763.5	5,859.3			6.17	0.17	
8	2,498.7	2.550.3	51.6	6.53	0.53	65,540.2	66,311.1	777.0	6,285.0	6,332.7 6,378.1	47.91 45.35	5.91	-0.09	
7	2.550.3	2,598.5	48.2	6.30	0.30	66.311.1	67,072.2	767.1	6,332.9	6,425.5	46.32	6.02	0.02	
3	2,598.5	2.645.7	47.2	6.05	0.05	67.072.2	67.835.9	769.8	6,379.3	6,472.1	46.68	6.08	0.08	
1	2.645.7	2.693.5	47.8	6.14	0.14	67,835.9	68,604.6	767.3	6,425.5 6,472.1	6,518.7	46.73	6.05	0.05	
6	2,693.5	2,741.6	48.1	6.21	0.21	68,604.6	69,371.2	772.7			3.09	1.18	0.18	
9	2.385.5	2,388.4	3.0	1.12	0.12	57,653.8	57,910.2	262.6	6,172.2 6,206.4	6,175.1	3.16	1.20	0.20	
3	2,419.5	2,422.6	3.1	1.12	0.12	60,680.5	60,937.1	262.7	6,209.6	6,209.5	3.12	1.18	0.18	
2	2,422.6	2.425.6	3.0	1.13	0.13	60,937.1	61,195.2 61,449.5	264.2 260.4	6,212.7	6,215.5	3.00	1.15	0.15	
3	2,425.6	2.428.6	3.0	1.11	0.11	61.195.2	61,705.4	261.9	6,215.7	6.218.6	3.05	1.16	0.16	
7	2.428.6	2,431.6	3.0	1.11	0.11	61,449.5	51.834.3	261.4	5,980.7	5,989.7	9.14	3.50	0.50	
1	2,190.4	2.199.4	9.0	3.47	0.47	51,579.0	53,601.3	264.4	6.040.5	6.049.6	9.29	3.51	0.51	
5	2.251.5	2,260.5	9.0	3.41	0.41	53,343.0 53,601.3	53,858.7	263.4	6,049.8	6,058.7	9.06	3.44	0.44	
1	2,260.5	2.269.7	9.2	3.54	0.54	53,858.7	54.116.9	264.4	6,058.8	6,067.7	9.01	3.41	0.41	
3	2.269.7	2.279.1	9.4	3.59	0.59	49,007.9	49,264.5	262.7	5,901.4	5,910.1	8.85	3.37	0.37	
6	2.116.5	2,125.0 2.072.8	8.5 9.2	3.56	0.56	47,483.8	47,737.9	260.2	5,850.2	5.859.2	9.18	3.53	0.53	
9	2.063.6				1.08	71,916.4		254.5	6.681.3	6,699.3	17.94	7.05	1.05	
2	2.907.9	2.926.4	18.5	7.08 6.94	0.94	72,170.9	72,427.6	262.8	6.699.5	6,717.1	17.80	6.77	0.77	
8	2.926.4	2,944.1	17.8 18.7	7.28	1.28	72,170.9	72.686.0	264.4	6,717.5	6,734.8	17.50	6.62	0.62	
8	2,944.1	2.962.8	18.7	7.28	1.08	72,686.0	72,944.1	264.2	6.735.1	6,753.1	18.18	6.88	0.88	
4	2,962.8 2,981.4	2,981.4 3,000.0	18.6	7.25	1.25	72,944.1	73.203.7	265.7	6.753.4	6,771.3	18.01	6.78	0.78	
8				1.09	0.09	61,705.4	61,959.4	260.1	6.218.7	6.221.5	2.97	1.14	0.14	
8	2,431.6	2,434.5	1.2	1.93	0.09	65.034.2	65.091.3	63.2	6,256.6	6,257.9	1.45	2.29	1.29	
2	2,470.4	2.471.6 2.473.1	1.5	2.33	1.33	65.091.3	65.149.0	63.8	6.258.0	6,259.3	1.45	2.27	1.27	
	2,471.6	2,473.1	1.4	2.44	1.44	65,149.0	65.203.1	60.3	6,259.6	6.260.9	1.45	2.41	1.41	
1	2,474.5	2.474.5	1.3	2.35	1.35	65,203.1	65,257.0	60.0	6,261.0	6,262.2	1.43	2.39	1.39	
		2,155.6	2.2	3.57	0.57	50.031.3	50,084.3	59.1	5.938.6	5,940.9	2.43	4.12	1.12	
,	2,153.4 2,155.6	2,155.0	2.5	4.24	1.24	50.084.3	50,139.7	61.5	5,941.2	5,942.5	1.50	2.44	-0.56	
		2,158.1	2.2	3.78	0.78	50,139.7	50,195.3	61.7	5,943.8	5,945.9	2.25	3.65	0.65	
	2,158.1	2,162.5	2.2	3.59	0.59	50,195.3	50,249.6	60.6	5,946.3	5,948.3	2.16	3.56	0.56	
,	2.162.5	2,162.5	2.2	3.72	0.72	50,249.7	50,302.0	58.4	5,948.6	5.950.8	2.33	3.99	0.99	
			5.2	7.85	1.85	65,257.0	65,331.6	80.7	6,262.3	6.267.2	5.09	6.31	0.31	
2	2.475.8	2,481.0 2,485.4	4.4	7.80	1.80	65,311.6	65,368.0	62.4	6.267.3	6.271.5	4.34	6.95	0.95	
<u> </u>	2.481.0	2,485.4	4.3	6.90	0.90	65,368.0	65,426.9	65.0	6.271.6	6,275.6	4.12	6.33	0.33	
-	2,485.4	2.494.1	4.4	7.17	1.17	65.427.0	65.486.8	65.9	6.275.7	6.280.2	4.61	6.99	0.99	
1	2.489.7 2.494 1	2.494.1	4.6	7.85	1.85	65.486.7	65.540.2	59.5	6.280.2	6,284.7	4.63	7 77	1 77	
	2.434	2.430.7	7.0											





APPENDIX B

FOAM CONTROL SYSTEM OPERATION OVERVIEW

Extracted from Nordic Systems Inc. Mark II Computerized Foam Proportioning System Service Manual for U.S.A.F. P-19

Figure B-1 shows the simplified **foam control** functional diagram. The system objective is to mix foam from the **foam tank** with water from the **water tank** in the correct proportion to form a **solution**. The solution is sprayed onto the fire through the **roof turret**, **bumper turret**, **or handline**.

In the **automatic mode**, the **Foam Control System** continuously adjusts the foam flow to deliver the correct solution concentration. When the **main pump** is started, water flows through the **turret** or other discharge devices. This flow rate is measured by the **solution paddle wheel flow sensor**. The flow computer calculates the foam flow rate required to get the solution to the percentage set on the control panel. Usually this percentage is **3**%, but can be 0%, 1%, 3% or 6%. The computer opens or closes the **motorized metering valve** to adjust the mixture to the correct value.

The foam flow rate is measured by the foam paddle wheel flow sensor. From this sensor, the foam control computer determines the number of gallons of foam per minute flowing. The percentage of foam in the solution is determined by dividing the foam flow rate by the solution flow rate. If the actual percentage foam in the solution is too high, the computer activates the motorized metering valve in the "close" direction tending to reduce the foam flow. Conversely, if the actual percentage foam in the solution is too low, then the metering valve motor is activated to "open" the metering valve, increasing the foam flow rate. The duration that the motor is activated is in all cases a fraction of a second, from ten thousandths of a second to one fifth of a second. The exact duration depends on the difference between the actual and desired foam percentage as set on the foam control computer face plate.

The foam control computer monitors the flow sensors about twice a second and immediately adjusts the metering valve accordingly.

Some solution is pumped around the pump through a restriction known as an **eductor**. The eductor generates a low pressure or a suction at one of its ports. Foam is sucked from the foam tank through the eductor into the solution flow and thence back into the pump. This scheme produces foam with a uniform consistency. The process is known as the **"around the pump method"**. This process thoroughly mixes the foam and water into a homogeneous solution. Apart from the fraction that is circulated around the pump, the entire pump output is available for fire fighting by discharge through the roof turret and other discharge devices.

Since foam is drawn into the eductor by a vacuum, the **foam line** is a **low pressure** line with pressures below 10 psi above the metering valve and usually negative below. On the other hand the pump output piping, **the solution line**, is a **high pressure** line with pressures as high as 150 psi.

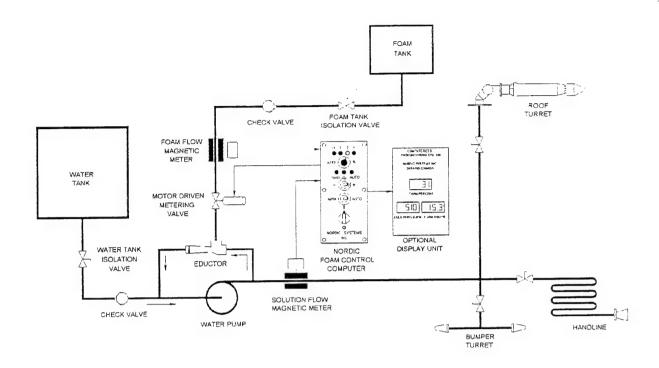


Figure B-1
Simplified foam control system including computer

COMPONENTS OF THE FOAM CONTROL SYSTEM

1 Check Valve

There are two **check valves**, one in the foam tank line and one in the water tank line. The check valves allow flow out from a tank but stop flow into a tank. Flow into a tank is an abnormal or fault condition which the check valves prohibit to avoid contamination of the tank contents. The **check valves** work automatically, and are **not controlled by the foam control system**.

2 Foam Valve

The foam valve shown in figure 1 is a pneumatically operated valve. Unless the foam valve is open, no foam can enter into the solution, only pure water will discharge from the turret. The **foam valve** is not controlled in any way by the foam computer. There are no electrical signals from the foam control computer to open or close the foam valve. The foam valve is manually activated by the operator through a three position pneumatic switch on the dashboard.

3 Foam Magnetic Flow Meter (originally a paddle wheel)

The foam magnetic flow meter (previously a paddle wheel) senses the flow of foam through the pipe from the foam tank to the eductor. The eductor which is a narrowing in the pipe around the pump, produces a low pressure or suction at the foam inlet port, thus foam is drawn into this eductor port. As the foam flows, the flow meter generates an electrical signal which is sent to the foam control computer, which calculates the actual percentage foam in the solution. Once this calculation is complete, the computer knows whether the mixture is too rich, too lean, or just right. Based upon the calculation, the computer adjusts the foam flow rate to the desired amount by opening or closing the motor driven metering valve. If the flow rate is too slow, the metering valve motor rotates the valve to increase the opening through which foam can flow. If the flow rate is too high, the metering valve is rotated to reduce the opening through which the foam can flow.

4 The Metering Valve

The **metering valve** is used to ensure that a measured volume flows through it. It consists of a ball valve driven by an electric motor, coupled through a reduction gear. This increases the motor torque or turning power and reduces its speed, both desirable properties in this application.

The motor is driven directly from the vehicles 24 Volt battery. Since it is a DC motor, reversing the polarity reverses the direction in which the motor rotates. Reversing the motor polarity is controlled by the computer to open/close the valve, thus increasing/decreasing respectively the foam percentage in the solution. Despite the gear reduction, the motor spins the metering valve so quickly that the valve can rotate from full off to full on in a couple of seconds. The computer attempts to maintain the foam percentage within one tenth of one percent of the selected value. In order to control the foam percentage in the solution to better than one tenth of a percent, the metering valve motor is pulsed as short as twenty thousandths (20/1000) of a second. For the pulse duration, the full battery voltage is applied to the motor. The average voltage varies widely depending on the duty cycle.

Needless to say, it is crucial that the metering valve and motor drive turn freely without sticking or jamming otherwise these very short duration control pulses will produce no valve correction and the foam control system will loose its "fine touch" or in the worst case, cease to operate at all. The metering valve requires the most attention and service of all the components in the system.

5 Eductor

The eductor produces suction when solution pumped "around the pump" is forced to flow through a restriction or narrowing in the pipe diameter. This low pressure, sometimes loosely called a vacuum, sucks foam concentrate from the foam tank into the eductor where it mixes with the water based solution. The rate at which foam is drawn into the eductor is controlled by the foam control computer. The foam control computer opens or closes the metering valve to maintain the solution foam concentration at the desired value. There are no moving parts in the eductor, it is simply a precisely shaped restriction in the pipe with a duct near the point where the restriction is greatest. The restriction is

shaped like the cross section of an aircraft wing. The restriction forces the fluid to increase in velocity (venturi effect) and in so doing, its pressure must fall, creating suction.

6 Main Pump

The **main pump**, when engaged by the operator, is driven by the vehicle engine. It provides the pumping action for the entire system. The pump consists primarily of an **impeller** which is spun by the vehicle motor to force solution out the discharge ports.

7 Solution Magnetic Flow Meter (originally a paddle wheel flow sensor)

This is similar to the foam flow sensor except that the flow rates are usually a least fifteen times greater. With the roof turret active, the solution flow rate is typically about 500 GPM while the foam flow rate would be 30 GPM for 6% foam solution. The solution magnetic flow meter would normally operate at pressures around 150 PSI, while the foam magnetic flow meter is experiencing a pressure from a foam column no more than six feet high, which creates a head of less than 3 PSI. This is because the foam is **gravity fed** to the foam metering valve and sucked through the metering valve by the eductor vacuum. The foam tank is not pressurized.

8 Main Turret Valve

The **main turret valve** is a pneumatically operated valve which the operator uses to turn on the main turret. When the operator activates a switch on the turret handle, compressed air is applied to the valve where it energizes a piston to fully open the main turret valve. This valve is either full open or shut off, it cannot be used to modulate the solution flow through the turret. The dispersion or shape of the turret discharge is controlled by the operator through a foot switch in the cab, near the accelerator pedal.

The main turret valve is not controlled or monitored by the foam control computer. It is operated independently of the computer by the operator. The foam control computer, in automatic mode, will adjust to the actual flow from zero to maximum flow rate. The computer adjusts the metering valve in response to demand, which may come from any or all the discharge nozzles.

9 Main Turret

The main turret is the **primary discharge device** for the vehicle. It is designed to mix the solution with the correct amount of air to give the solution the consistency to extinguish the fire under attack.

10 Water Tank

The water tank 1000 gallons, which will supply the turret for about two minutes operating at 500 GPM. The water is gravity fed from the water tank to the main pump. The tank is not pressurized.

11 Foam Tank

The foam tank holds the concentrated foam for mixing with water to produce the desired percentage solution. The tank holds about 130 gallons of concentrated foam. At normal operating solution percentage, 3%, there is enough foam in the tank to satisfy four

tanks of water, so that the foam tank would only have to be filled every fourth trip to refill the water tank. Like the water tank, the foam tank is not pressurized, its contents flow out under gravity.

12 Foam Control Computer

The computer, figure B-2, gets its power from the **truck battery** through a power cable. The computer receives the solution flow rate from the solution flow sensor and the foam flow rate from the foam flow sensor, with this information the foam percentage rate can be calculated. A cable connects computer power to the metering valve providing high currents to open/close the valve. An additional cable provides metering valve position to the computer. Limit switches on the metering valve indicate when it is fully open or fully closed. This limit switch information is critical to the computer which will not attempt to control the foam unless the limit switches are functioning.

The control computer can operate in **manual or automatic mode**. In **manual mode**, the operator activates the metering valve directly. This is done through a spring loaded, center off, momentary contact switch. If the switch is pushed in the "+" direction, the valve rotates in the **open** direction, while a push in the "-" direction rotates the valve in the **close** direction. The longer the switch is held, the greater the valve response. The valve will **remain in the position** it is in when the switch is released (**returns to the center position**). When the limit switches indicate that the valve is fully open/closed, no further motion in the respective direction is permitted. Circuits in the controller **chop the current** applied to the metering valve to slow down the speed of operation thereby making it feasible for the operator to accurately control the valve.

In **automatic mode**, the foam control computer automatically monitors the solution flow. It computes the required foam flow based on the percentage foam setting on the console and the actual solution flow rate. If the actual foam percentage in the solution is too low, it opens the metering valve in proportion to the error. The metering valve motor rotates the valve in a direction to increase the opening through which foam can flow. If the flow rate is too high, the metering valve is rotated in the direction to reduce the opening through which the foam can flow. This monitoring and **adjustment** is carried out about **two times per second**.



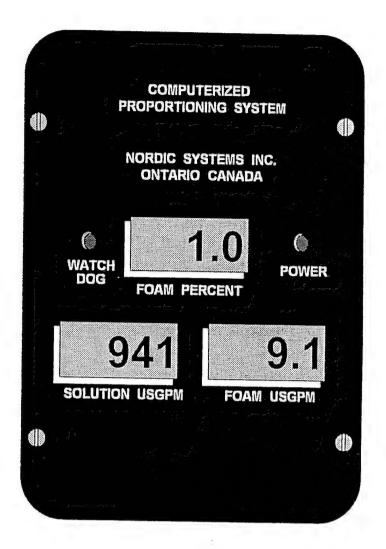
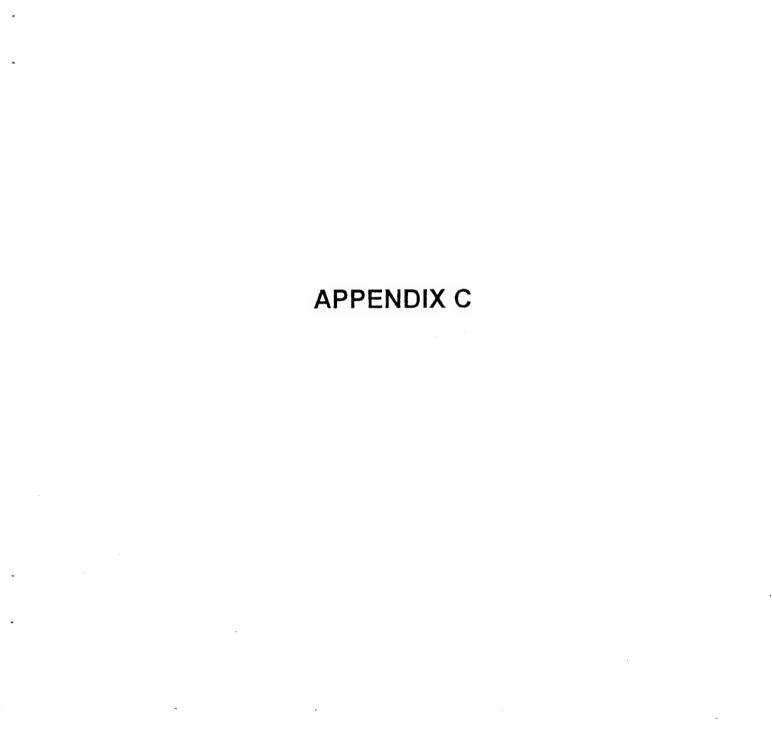


Figure B-2

NORDIC Mark IIA Computerized Foam Proportioning System Dashboard Control and Display Panel



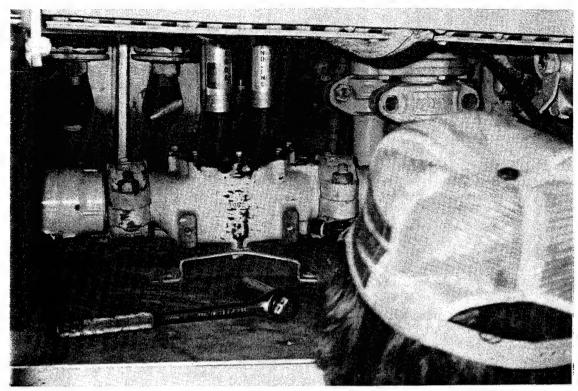


Photo 1 Original Around-the-pump metering System

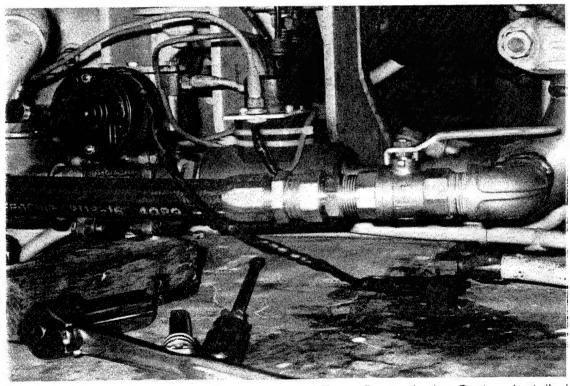


Photo 2 NORDIC Mark IIA Computerized Foam Proportioning System Installed

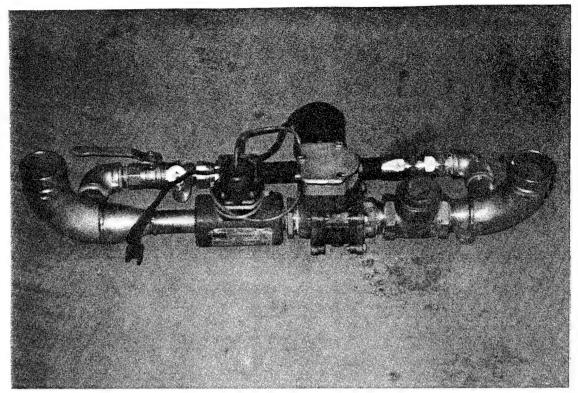


Photo 3 NORDIC Mark IIA Computerized Foam Proportioning System Valves and Plumbing

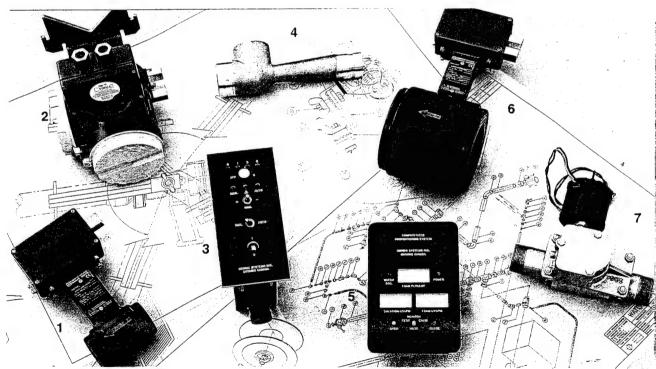


Photo 4 NORDIC system with magnetic flow meters

1. Foam concentrate magnetic flow meter sensor 2. Magnetic flow meter transmitter 3. Computer
4. Eductor 5. Optional digital display 6. Solution magnetic flow sensor 7. metering valve



APPENDIX D

MARK IIA AQUEOUS FILM FORMING FOAM
PRECISION METERING SYSTEM
PRODUCT EVALUATION PLAN
JUNE 1992



AIR FORCE CIVIL ENGINEERING SUPPORT AGENCY

TYNDALL AIR FORCE BASE, FLORIDA 32403

D - 1

MARK IIA AQUEOUS FILM FORMING FOAM PRECISION METERING SYSTEM PRODUCT EVALUATION PLAN JUNE 1992

Revisions to this Evaluation Plan involving changes in scope or resources will be approved by the Chief of Fire Protection, HQ AFCESA.

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ABSTRACT

This plan specifies procedures to evaluate a commercially developed aqueous film forming foam (AFFF) metering system installed in an A/S32P-19 firefighting vehicle. The system can be controlled by the vehicle operator without dismounting or relinquishing control of the vehicle. Headquarters Air Force Civil Engineering Support Agency, Firefighting and Facilities Branch, has overall responsibility for program management. The Responsible Test Organization, HQ AFCESA/RACF, will conduct the evaluation at Tyndall AFB, Florida, at Fire Research Facility #1. One off-the-shelf AFFF metering system manufactured by Nordic Systems Inc. will be evaluated. The primary focuses of this evaluation are to examine the metering accuracy, system performance, operational effectiveness, and suitability of the AFFF system. The results of the evaluation will be used to support a decision to modify existing firefighting apparatus.

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ABBREVIATIONS

AQUEOUS FILM FORMING FOAM AFFF

AIR FORCE REGULATION AFR

OPERATIONAL AVAILABILITY Αo

CRASH FIRE RESCUE CFR

DEPARTMENT OF DEFENSE DOD

DEFENSE SWITCHING NETWORK DSN

GALLON gal

GALLONS PER MINUTE gpm

HEADQUARTERS AIR FORCE CIVIL ENGINEERING SUPPORT HQ AFCESA

AGENCY

IN ACCORDANCE WITH IAW

ITI LIMITED TECHNICAL INSPECTION

MISSION CAPABLE MC MEAN DOWN TIME MDT

MEASURE OF EFFECTIVENESS MOE

MEAN TIME BETWEEN MAINTENANCE MTBM

NATIONAL FIRE PROTECTION ASSOCIATION NFPA

NOT MISSION CAPABLE NMC

A/S32P-19 CRASH FIRE RESCUE VEHICLE P-19

RELIABILITY, MAINTAINABILITY, AND AVAILABILITY RESPONSIBLE TEST ORGANIZATION RM&A

RTO

SECTION I

- 1.1 <u>Purpose</u>. Headquarters Air Force Civil Engineering Support Agency (HQ AFCESA), Firefighting and Facilities Branch (RAAE), will manage a product evaluation to verify metering accuracy, operational effectiveness, and suitability of the Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System (hereafter called Mark IIA). The evaluation will be conducted by the Responsible Test Organization (RTO), HQ AFCESA/RACF, from 13 July through 9 November 1992, at Fire Research Facility #1, Tyndall AFB, FL. HQ AFCESA/RAAE will use the data collected to compare the aqueous film forming foam (AFFF) metering accuracy, foam discharge pattern, and hydrocarbon fire extinguishing capability of the Mark IIA with two other systems: the orifice plate system currently employed on the P-19 and the Hypro Corporation's metering system previously evaluated by RACF. The results of the evaluation will support a decision to retrofit Air Force AFFF firefighting apparatus. If applicable, the Department of Defense (DOD) could use the results of the evaluation for other firefighting vehicles.
- 1.2 System Description. The Mark IIA AFFF metering system is a computerized foam proportioning system. Nordic Systems Inc. personnel will install and calibrate the Mark IIA system on RACF's P-19 firefighting vehicle used in the evaluation and provide operator and maintenance training to evaluation participants. The system is government property and will be available for other test purposes if required. During the Mark IIA installation, Nordic Systems Inc. personnel will require some assistance from RACF personnel to install sight gauges on the water and AFFF tanks, and provide information on the P-19 water The Mark IIA system consists of: a computer, foam flow meter, solutions flow meter, foam control valve, a self-contained digital read-out unit, and associated wiring and electrical connectors. The Mark IIA computer program has been modified to meet current USAF objectives to provide foam in concentrates of 1.0%, 3.0%, and 6.0% at flow rates between 60 and 500 gallons per minute (GPM). The AFFF dispensing ratio of the Mark IIA system is switch selectable over a range of 0-6.0% AFFF by the operator from the cab of the vehicle. After the AFFF reservoir is serviced with foam concentration, the vehicle operator can adjust the Mark IIA the match the AFFF concentration in the reservoir.

- 1.3 <u>Background</u>. The DOD currently uses AFFF concentrates formulated and mixed with water in ratios of 3 and 6 percent, using an around-the-pump proportioning system with fixed orifices. Common fire protection community terminology refers to an AFFF concentrate designed to be mixed with water at a ratio of 3% AFFF to 97% water as "3% AFFF". A "6% AFFF" concentrate contains approximately one-half of the surfactant and other active ingredients as 3% AFFF concentrate per unit volume and, consequently, is referred to as "less concentrated". When mixed with water at their designed ratios, both types AFFF/water mixture are essentially the same. By using 1.0% AFFF concentrate (as compared to 3% and 6%), agent conservation and extended firefighting capability should be realized. Six percent foam concentrate will be evaluated to provide system performance data in case situations arise again where the Air Force "borrows" 6.0% foam from the Navy during Desert Storm. This product evaluation will be accomplished as part of a continuing effort to identify an AFFF system capable of metering foam accurately at 1% concentration.
- 1.4 <u>Objectives</u>. The primary objectives of this evaluation are to verify the AFFF metering accuracy and consistency of the Mark IIA system in the P-19 firefighting vehicle. The secondary objectives are to determine the effects of the Mark IIA system on the foam discharge pattern and the ability to produce quality foam. This evaluation will assess the Mark IIA system performance, operational effectiveness, and suitability for use with the P-19. The specific objectives are:
- 1.4.1 Objective E-1. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- 1.4.2 Objective E-2. Assess the operational performance of the Mark IIA system installed on the P-19.
- 1.4.3 Objective S-1. Assess the compatibility of the Mark IIA system installed on the P-19 with firefighting operations.
- 1.4.4 Objective S-2. Assess the adequacy of technical data provided with the Mark IIA system.
- 1.4.5 Objective S-3. Assess the Mark IIA system Reliability, Maintainability, and Availability (RM&A).

- 1.5 Evaluation Concept and Scope.
- 1.5.1 Prior to modifying the P-19 vehicle with the Mark IIA system, the RTO will demonstrate the AFFF metering accuracy, foam discharge pattern, and foam quality of the existing orifice plate system. The results will be documented, and a performance baseline created for comparison with the Mark IIA system. After the orifice plate system has been baselined, the Mark IIA system will be installed on the same P-19 vehicle and the same AFFF metering accuracy, foam discharge pattern, and foam quality data will be collected on the Mark IIA.
- 1.5.2 Evaluation Conditions. The evaluation participants from RACF/ARA will be task qualified firefighting and maintenance personnel. Fire suppression capability demonstrations will consist of a 300 gallon hydrocarbon fire set in the RACF Fire Research Facility #1 pit. At the conclusion of each foam percentage evaluation, the AFFF metering accuracies and foam discharge patterns will be measured using the sight gauges and spray measurements to evaluate the repeatability of the Mark IIA system to consistently provide 1.0%, 3.0%, and 6.0% AFFF.
- 1.5.3 Procedures. AFFF metering accuracy evaluation data requirements are outlined in the data forms 6, 7, and 8. Foam discharge pattern evaluation procedures and data requirements are outlined in NFPA Standard 412. General firefighting practices and procedures as outlined in Air Force Regulation (AFR) 92-1, Fire Protection Program, will be followed. The safety and protection of personnel and equipment will take priority over accomplishing any evaluation task or objective.
- 1.5.4 Authority for the Mark IIA system product evaluation is in PMD 8028(9), dated 10 May 1991. This evaluation will be conducted as directed in AFR 80-14 and AFR 55-43, and a final report will be released for publication no later than 45 calendar days after the final evaluation data are collected processed.
- 1.5.5 Mark IIA system reliability data will be reported as mature system point data since the system is commercially available (off-the-shelf).

SECTION II OBJECTIVES AND EVALUATION METHODOLOGY

- 2.1 <u>General Method of Accomplishment</u>. The capabilities of the Mark IIA system installed on a P-19 fire truck will be assessed for AFFF metering accuracy, foam discharge pattern, and fire suppression of controlled aircraft type hydrocarbon fires set in RACF's Fire Research Facility #1. The data on system performance, operational effectiveness and suitability will be recorded and reported as point data due to the relatively short evaluation period. Incompatibilities between the system and operational requirements will be documented on data forms provided and will include the procedures followed leading to the noted incompatibility, suggested corrective procedures, suggested hardware changes, and actions required to continue with operations.
- 2.2 <u>Objective E-1</u>. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- 2.2.1 Measure of Effectiveness (MOE) and Evaluation Criterion. The MOE is noninterference. The criterion is no mutual interference between or among the P-19 and the Mark IIA system.
- 2.2.2 Method. Nordic Systems technicians will be assisted by RACF personnel during the installation and calibration of the Mark IIA system in the P-19 evaluation vehicle. They will perform a limited technical inspection (LTI) and functionally operate the Mark IIA modification prior to beginning the evaluation. RACF/ARA/BDM personnel will compare the installed hardware and components to the technical data package provided by Nordic Systems Inc. to verify completeness. The orifice plate system removed from the P-19 will be inventoried, inspected for completeness and apparent serviceability, and stored by RACF.
- 2.2.3 Data Requirements.

Element
Inputs from Evaluation Manager
Inputs from Evaluation Participants

Source
Data Forms 1 and 3

- 2.2.4 Data Collection and Processing. Evaluation participants will collect, compile, and categorize data during the evaluation. The Evaluation Manager will have primary responsibility for ensuring the accuracy and validity of the data collected. Data forms will be completed as required. The evaluation data will be the basis of the evaluation report.
- 2.3 Objective E-2. Assess the operational performance of the Mark IIA system installed on the P-19.
- 2.3.1 MOE and Evaluation Criteria. The MOE is Mark IIA system performance. The criteria are that the Mark IIA system consistently repeat metering accuracy, foam discharge patterns, and fire suppression capabilities.
- 2.3.2 Method. The P-19 vehicle water and AFFF tanks will be calibrated following the Firefighting Vehicle Fluid Calibration Procedures in data form 5. The P-19 and Mark IIA systems will be serviced and prepared for use in accordance with applicable technical manuals. After preparation for use, the P-19 and Mark IIA systems will be operated to dispense AFFF ten times from each turret/nozzle (roof, bumper, and handline) for 60 seconds with 1%, 3%, and 6% AFFF. After each

60 second dispensing operation, the water and AFFF tank quantities will be recorded using fluid sight gauges on the vehicle to determine the amounts used. This will be accomplished to compute the Mark IIA system metering accuracy and to determine repeatability with the various AFFF concentrations. The handline is included to determine the Mark IIA's ability to accurately meter AFFF at the lower flow rate of 60 GPM. To determine AFFF dispersal pattern consistency, the procedures in NFPA Standard 412, paragraph 4-1, Turret Ground Pattern Test, will be followed. The Mark IIA system will then be employed IAW standard firefighting procedures to extinguish 300 gallon pit fires to demonstrate fire suppression capabilities with 1%, 3%, and 6% AFFF concentrations. During dispensing operations, special attention will be given to the Mark IIA system performance. Incompatibilities between the Mark IIA system and the P-19 fire truck or other CFR equipment will be recorded in detail. Likewise, enhanced capabilities due to the Mark IIA system performance or its interface with other CFR equipment will be recorded in detail.

During the live fire events, the Evaluation Manger will insure compliance with the safety procedures identified in Section IV.

2.3.3 Data Requirements.

Element

Source

Inputs from Project Manager

Data Forms 1 through 8

Inputs from Evaluation Participants

- 2.3.4 Data Collecting and Processing. Evaluation participants will collect. compile, and categorize data during the evaluation. The Evaluation Manager will have primary responsibility for ensuring the accuracy and validity of the data collected. Data forms will be completed as required. The evaluation data will be the basis of the evaluation report.
- 2.4 Objective S-1. Assess the compatibility of the Mark IIA system with the P-19 firefighting vehicle.
- 2.4.1 MOE and Evaluation Criterion. The MOE is compatibility among and between all components of the Mark IIA system and the P-19 in the operational environment. The criterion is that the performance of the Mark IIA system neither prevent nor hinder successful performance of any evaluation event.
- 2.4.2 Method. The Mark IIA system will be employed as described in paragraph 2.3.2 and maintained IAW the operational concept and the manufacturer's technical data. The evaluation participants will be briefed to be alert for any actual or foreseeable compatibility problems between and among the components. evaluation participants will notify the Evaluation Manager of any observed or experienced compatibility problems. The Evaluation Manager will record their comments in the Evaluation Manager's Log.
- 2.4.3 Data Requirements.

Element Inputs from Project Manager Inputs from Participants

Source Data Forms 1,2,3 and 4

2.4.4 Data Collection and Processing. Same as Paragraph 2.2.4.

- 2.5 <u>Objective S-2</u>. Assess the adequacy of the vendor provided technical manuals for the Mark IIA system.
- 2.5.1 MOE and Evaluation Criteria. The MOE is the adequacy of the technical manuals as judged by evaluation participants. The criteria are that the documents be written so a task-qualified technician can readily understand and follow the procedures and, by following the procedures, achieve the intended outcome.
- 2.5.2 Method. During this evaluation, participants will use the vendor provided technical manuals. After each evaluation event, the participants will indicate, on data forms and maintenance logs, any difficulties that prevented or hindered successful task performance. The Evaluation Manager will record reported problems, pertinent observations, and comments in the Evaluation Manager's Log.
- 2.5.3 Data Requirements.

Element
Inputs from Project Manager
Inputs from Participants

Source
Data Forms 1,2,3 and 4
System Operator's Manual

- 2.5.4 Data Collection and Processing. At the conclusion of the evaluation, the team will compile the collected data. Technical manual deficiencies will be reviewed and verified prior to inclusion in the evaluation report. The Evaluation Manager will be responsible for ensuring reported technical manual deficiencies are clearly and completely explained.
- 2.6 <u>Objective S-3</u>. Assess the Mark IIA system Reliability, Maintainability, and Availability (RM&A).
- 2.6.1 MOE and Evaluation Criterion. The MOE is system RM&A. There is no criterion established for this system.
- 2.6.2 Method. The system will be employed as described in this section. The Evaluation Manager and participants will record system failure and repair data. These data will be used to calculate system point RM&A rates for the evaluation period.
- 2.6.3 Data Requirements. Same as paragraph 2.5.3.
- 2.6.4 Data Collection and Processing. The evaluation participants will collect, compile, and categorize data during the evaluation. The Evaluation Manager will have primary responsibility for ensuring the accuracy and validity of the data collected. Failures will be recorded and reported in chronological order on data forms. The failure data will be used to calculate the Mean Time Between Maintenance (MTBM), Mean Down Time (MDT), and Operational Availability (Ao) as follows:

MTBM = TOTAL OPERATING TIME

TOTAL NUMBER OF MAINTENANCE EVENTS

MDT = TOTAL MAINTENANCE REPAIR TIME TOTAL NUMBER OF REPAIR ACTIONS

 $Ao = \frac{POSSESSED TIME - DOWN TIME}{POSSESSED TIME} X 100$

Maintenance Events for MTBM calculations are defined as any maintenance action required to correct a Mark IIA system or component malfunction which renders it not mission capable. P-19 fire truck failures will be recorded but not charged to the Mark IIA system RM&A rates. The total operating hours shall be the sum of the hours taken from the Operational Status Log and will include the total time the system was in use. The time the system is not serviceable due to a failure will not be included as operating hours. The MDT will not include time lost due to the non-availability of replacement components. The system developed for this evaluation was not provisioned with spare/replacement components; therefore, the time required to arrange for the replacements from the vendor will not be charged against the system. Repair time will count only the time required to troubleshoot and physically repair the actual failure. The Ao will be expressed as the percentage of time the system is available for use with respect to the total time required for use.

SECTION III MANAGEMENT AND RESOURCES

3.1 Management Relationships.

3.1.1 HQ AFCESA/RAAE will exercise overall program direction and provide funding for the Nordic Systems Inc. Mark IIA AFFF computerized metering system evaluation. HQ AFCESA/RACF, the Responsible Test Organization (RTO), will conduct the evaluation and provide the data collected to RAAE for analysis and reporting.

3.1.2 HQ AFCESA/RACF will organize evaluation events, collect and correlate data, and provide security, storage, and personnel support for the evaluation. Upon completion of the evaluation, RACF with RAAE will publish an evaluation report within 45 days of receipt of the compiled evaluation data.

3.2 Key Personnel. Table 1 lists personnel who are responsible for evaluation planning, implementing, and reporting.

	TABLE 1.	KEY PERSONNEL	
<u>Title</u>	Name/Grade	Organization	<u>Phone</u> (DSN)
Project Sponsor	Mr Laird	HQ AFCESA/RAAE	523-6290
Project Advocate	CMSqt Reyff	HO AFCESA/DF	523-6156
Project Manager	Mr Grimm	HO AFCESA/RAAE	523-6303
Evaluation Manager	Mr Vickers	HO AFCESA/RACF	523-3734
Project Engineer	Mr Pike	HQ AFCESA/DFE	523-3742
Technical Ădvisor	Mr Wilson	ARA	523-3169
Technical Advisor	Mr Dees	ARA	523-3169

- 3.3 Resources. HQ AFCESA/RACF will provide facilities, consumables, equipment, and personnel to support this evaluation.
- 3.3.1 Evaluation Support. Table 2 lists evaluation support requirements.

TABLE 2. EVALUATION REQUIREMENTS

EQUIPMENT ITEMS	INCHENTS
QUANTITY MODIFIED A/S32P-19/Mark IIA PORTABLE VIDEO CAMERA 35 MILLIMETER STILL CAMERA STOPWATCH 100-FOOT MEASURING TAPE	1 (full time) 1 (during events) 1 (during events) 2 (during events) 1 (during events)
CONSUMABLE ITEMS QUANTITY FUEL (SUITABLE FOR LIVE FIRE EVENTS) 1/2-INCH VIDEO TAPE 35 MILLIMETER FILM (COLOR SLIDES and PRINTS) WATER AFFF 1% 3% 6%	800 gallons 5 each 5 rolls 18,000 gallons 250 gallons 600 gallons 1100 gallons
FACILITIES MAINTENANCE BAY STORAGE BAY FIRE PIT	l (as required) l (as required) l (as required)

3.3.2 The Evaluation Manager is authorized to contact Nordic Systems Inc. directly, as necessary, to aid in accomplishing this evaluation; however, he may not offer to purchase or obligate the Air Force in any way. This must be clearly stated in all communications with commercial vendors. As soon as it is practical, the Evaluation Manager will notify HQ AFCESA/DF and RAAE of any reportable evaluation related personnel injury or catastrophic system failure, caused by or relating to the use of the P-19/Mark IIA system. At the completion of the evaluation, the Evaluation Manager will collect and compile the data required to publish an evaluation report. HQ AFCESA/RAAE will prepare the evaluation report.

3.4 Release of Information.

- 3.4.1 HQ AFCESA/PA, DSN 523-6476, is responsible for information coverage of this evaluation. Clearance of information will be in accordance with AFR 190-1, Public Affairs Policies and Procedures, Chapters 6 and 9. News releases, if any, will spotlight the evaluation purpose, equipment, methods, and participating personnel. No value judgement will be made.
- 3.4.2 The Evaluation Manager is responsible for informing HQ AFCESA/DF and RAAE of any incident or mishap. The releasing authority for information on any incident or mishap is HQ AFCESA/PA, through the safety office of the evaluation location or the base public affairs officer, after coordination with the HQ AFCESA/CC. Releases will be made in accordance with AFR 190-1.

SECTION IV

4.1 <u>Purpose</u>. General firefighting practices and procedures are outlined in Air Force Regulation (AFR) 91-1, <u>Fire Protection Program</u>, will be followed throughout the evaluation. The safety and protection of personnel and equipment takes priority over accomplishing any evaluation objective. Every effort will be made to prevent deviating from preplanned actions, and standard operating practices and procedures. Deviations may only be authorized by the evaluation manager with the concurrence of the AFCESA safety officer. This Safety Plan establishes the safety areas for live fires using partial percentage AFFF. Live fires will be conducted at the AFCESA Fire Research Facility #1. This document contains detailed safety rules which govern the conduct of this evaluation series. The Evaluation Manager will act as Supervisor of Fire Test (SOFT) and will ensure adherence of all safety policies. Before conducting any live fires at the Fire Research Facility, the Base Fire Department Communications Center will be notified. The following documents are applicable to this test:

AFOSH 127-40 & 42, Emergency Eye Wash AFOSH 127-11 & 50, First Aid Kits AFOSH 127-31, Personal Protective Clothing and Equipment AFR 92-1, Paragraph 4-14, Safety Equipment for Fire Fighters AFR 127-4, Accident Reporting

4.2 <u>Overall Safety Responsibility</u>. HQ AFCESA/RACF, as Evaluation Manager, is responsible for enforcing the overall safety program for the evaluation. The Evaluation Manager or his designated representative will act as the Safety Officer during all fire events at the test site.

4.3 General Safety.

- 4.3.1 <u>Safety Briefing</u>. The Evaluation Manager will inform all test personnel on known safety hazards associated with this test and test site. Supervisors will, in turn, inform their personnel on these hazards.
- 4.3.2. <u>Visitors</u>. Visitors will be permitted at the test site only with the approval of the Evaluation Manager. Visitors will be instructed on applicable safety regulations.
- 4.3.3. <u>Individual Safety Responsibility</u>. Careful attention to potential hazards associated with fire testing must be stressed at all levels of responsibility. The purpose of the safety rules outlined herein is to present the most important elements in experimenting with controlled fires. These rules do not cover all the possible hazards which may occur at the site. As new problems arise, new safety measures must be established. This Safety Plan must be strictly adhered to by all personnel and enforced by all supervisors.
- 4.3.4 <u>First Aid</u>. A first-aid kit will be maintained at the site and all personnel will be informed on its location.
- 4.4 Accident Reporting (Emergency).
- 4.4.1 <u>Scope</u>. The purpose of this procedure is to ensure expedient handling and care of personnel injured in an accident or disaster. All post-emergency reporting and investigation of an accident will be performed in accordance with applicable Air Force regulations.

- 4.4.2 <u>Responsibility</u>. Each person involved in this program must be familiar with the emergency reporting procedures established by this plan and immediately implement these procedures in the event of an accident. The Evaluation Manager will ensure that all supervisors and subordinates are familiar with this procedure.
- 4.4.3 <u>Emergency Reporting Procedures</u>. In the event of an accident at the test site, the following procedures will be followed:

a. The Evaluation Manager will direct appropriate first aid. Caution will

be exercised to prevent aggravation of an accident-related injury.

b. Tyndall Air Force Base Hospital Ambulance Service will be notified by calling extension 911. The nature of the accident, including apparent condition of injured personnel and the location of the test site, will be reported to the medical personnel. The Evaluation Manager or his designated representative will decide whether to transfer the injured directly to a hospital or to request emergency ambulance support.

c. The Evaluation Manager or his designated representative will determine the seriousness of the accident. If the accident is not serious enough to require emergency hospitalization or ambulance service, the injured person will

be taken to a doctor or hospital by normal means of transportation.

d. All accidents requiring emergency treatment or first aid must be reported to the AFCESA Safety Officer.

- 4.5 Fire Prevention, Reporting, and Emergency Procedures.
- 4.5.1 <u>Responsibility</u>. The Evaluation Manager will be responsible for the implementation of the procedures established by this plan. All on-site personnel must be completely familiar with these procedures to ensure proper response to an emergency.
- 4.5.2 <u>Fire Prevention Procedures</u>. The procedures listed in Check List #1 are to be followed in an effort to reduce chances of an uncontrolled fire.
- 4.6 <u>Test Site Location</u>. All fire evaluations will be conducted at the 100 foot AFCESA Fire Research Facility #1, located on Farm Dale Road. These tests will be conducted in accordance with AFCESA Office Instruction dated 7 April 1988, entitled "Live Fire Demonstration/Tests". The following checklist will be used prior to conducting live fire evaluations.

CHECK LIST #1 TO BE USED BEFORE CONDUCTING LIVE FIRES AT FIRE RESEARCH FACILITIES NO. 1

DATE:	
VERIF	IED PROCEDURES
	Inform all personnel on proper safety precautions.
	All personnel at the test site are needed to support the test or an
	approved visitor?
	Inform all personnel on accident and fire reporting procedures. Radio or telephone communications available?
	Radio or telephone communications available?
	Inform all personnel of the telephone numbers for the ambulance and fire
	department. Ensure a first aid kit is available. Ensure an emergency eye wash station is available. Ensure all fuel valves are closed and there are no fuel leaks prior to fuel ignition.
	Ensure a first and kit is available. Freume an emergency eye wash station is available
	Ensure all fuel valves are closed and there are no fuel
	leaks prior to fuel ignition.
	Secure area prior to igniting fire.
Commu Cente	Notification. Before conducting a fire test, notify the Fire Department nications Center at Extension 3-2884. The Fire Department Communications r will need an estimate of the duration of the live fire tests. The nications Center will be requested to notify the following: a. Command Post - 3-2155 b. Air Traffic Control Tower - 3-4553 c. Base Hospital - 3-7514 d. Security Police - 3-2028 e. Division of Forestry - 3-2641 f. Base Weather - 3-2856

ANNEX 1

DATA FORMS

AN ABBREVIATED SET OF DATA FORMS ARE INCLUDED ON THE FOLLOWING PAGES

DATA FORM #1 EVALUATION MANAGER'S LOG

DAT	E	EVENT & COMMENT

		DATA FORM # 2 FAILURE LOG
DATE	FAILURE (CLASSIFICATION / CAUSE / CORRECTIVE ACTION
		DATA FORM # 3 EVALUATION EVENT LOG
DATE	EVENT	COMMENT
DDITIC	DNAL COMMENTS:	

DATA FORM # 4 OPERATIONAL STATUS LOG

DATE	TIME	STATUS	COMMENT
-			
		L	and the second s

STATUS CODES:

MC - MISSION CAPABLE, THE SYSTEM IS READY FOR USE.

NMC - NOT MISSION CAPABLE, THE SYSTEM CANNOT BE USED DUE TO A HARD FAILURE.

NMR - NOT MISSION READY, THE SYSTEM IS OUT OF SERVICE FOR A SCHEDULED INSPECTION OR SERVICING (NOT A SYSTEM FAILURE). "NMR TIME" WILL BE COUNTED AS "MC TIME" FOR PURPOSES OF CALCULATING SYSTEM RM&A DATA UNLESS A FAILURE IS DISCOVERED DURING THE MAINTENANCE ACTION.

DATA FORM # 5 FIRE FIGHTING VEHICLE FLUID CALIBRATION PROCEDURES

- A. Water Tank Calibration.
- 1. Ensure that water tank is empty.
- Ensure that the vehicle is parked on a level surface throughout tank calibration procedures.
- Using a liquid flow meter, fill tank in 50 gallon increments, to its 1,000 gallon capacity, and calibrate a tank level indicator (dip stick) at 50 gallon increments.

DATA SHEET WATER TANK

- B. AFFF Tank Calibration.
- 1. Ensure that AFFF tank is empty.
- Ensure that the vehicle is parked on a level surface throughout tank calibration procedures.
- Using a liquid flow meter, fill AFFF tank in 5 gallon increments, to its 130 gallon capacity, and calibrate a tank level indicator (dip stick) at 5 gallon increments.

DATA SHEET AFFF TANK

Date: Vehicle R Test Conductors:	legistration Number:	Date: Evaluator:	Vehicle	Registration	Number:
Fill Water Point Gallons	Water Depth	Fill Point	AFFF Gallons	AFFF <u>Depth</u>	
1		1 2			
3 4 5		3 4 5			
6		6 7			
9		8 9 10			
11	\equiv	11 12			
13 14 15	_	13 14 15			
16 17	\equiv	16 17			
18 19 20	=	18 19 20			

ALL METERING SHEETS IN ORIGINAL TEST PLAN INCLUDED 10 RUNS UNDER EACH CATEGORY

DATA FORM # 6 1% AFFF METERING TEST MATRIX AND DATA COLLECTION SHEET

TEST NO. <u>TURRET</u>	AFFF DISPENSING TANK TIME (sec)	WATER TANK START END	AFFF TANK START END	WATER USED	AFFF USED	RATIO	AMB. TEMP	TEST <u>DATE</u>
1-10 ROOF	1% AFFF 60							
1-10 BUMPER	1% AFFF 60							
1-10 RF/BMP	1% AFFF 60							
1-10 HNDLNE	1% AFFF 60							

DATA FORM # 7 3% AFFF METERING TEST MATRIX AND DATA COLLECTION SHEET

TEST NO. <u>TURRET</u>	AFFF DISPENSIN TANK TIME (sec	WATER TANK START END	AFFF TANK START END	WATER USED	AFFF USED	RATIO	AMB. TEMP	TEST DATE
1-10 ROOF	3% AFFF 60							
1-10 BUMPER	3% AFFF 60							
1-10 RF/BMP	3% AFFF 60							
1-10 HNDLNE	3% AFFF 60							

DATA FORM # 8 6% AFFF METERING TEST MATRIX AND DATA COLLECTION SHEET

TEST NO.	TURRET		DISPENSING TIME (sec)	WATER START	TANK END	AFFF START	TANK END	WATER USED	AFFF USED	RATIO	AMB. TEMP	TEST DATE
1-10	ROOF	6% AFFF	60							-101	-	
1-10	BUMPER	6% AFFF	60				-					
1-10	RF/BMP	6% AFFF	60									
1-10	HNDLNE	6% AFFF	60									

NOTE: RF/BMP = ROOF and BUMPER

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